

# Measurement of Ultrashort Vector Pulses From Polarization Gates by In-Line, Single-Channel Spectral Interferometry

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**Abstract**—The growing use of ultrashort laser pulses exhibiting time-varying polarization (vector pulses) demands simple and robust characterization techniques capable to perform measurements in a broad range of experimental and environmental conditions. Here, we present in-line, single-channel setup based on spectral interferometry to characterize ultrashort vector pulses. The use of a *bulk* interferometer based on birefringence is key for the stability and sensitivity of the technique, thus being simple and highly robust. The technique is used to measure vector pulses corresponding to polarization gates, which are used in many applications. Those results are validated by simulations. The technique here presented has a number of potential applications in nonlinear effects (e.g., transient birefringence and nonlinear phenomena with vector pulses).

**Index Terms**—Ultrafast lasers, ultrashort pulses, optical polarization measurements, vector pulses, polarization gate.

## I. INTRODUCTION

ADVANCES on laser technology are enabling the generation and use of pulses of light more and more complex, both on time (e.g., single-cycle pulses) and singular spatial distributions (e.g., ultrashort pulsed vortex, Bessel beams, etc.). In addition, there is a raising interest on ultrashort pulses exhibiting time-varying polarization (vector pulses) [1]–[4]. The use and analysis of vector pulses is a useful tool in the study of quantum wells properties [5], vector coherent control for selective isomerization of enantiomers [6]–[9] and the generation of THz pulses with time evolving polarization from IR vector pulses [7], to mention some examples.

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In the *attoscience* field, vector pulses are used to alter the high-order harmonic generation (HHG) process in gas. Because of the high sensitivity of the HHG on atoms to light polarization (when light polarization is not linear, HHG efficiency vanishes), ultrashort pulses with particular temporal evolving polarization, known as polarization gates (PG), are used to control the number of attosecond light bursts created in the process [10]–[12]. When applied to few-cycle pulses, the resulting vector pulses from the PG are able to generate isolated attosecond pulses through HHG [13]. In a different configuration, two non-collinear counter-rotating circularly polarized beams create a vector pulse that generates isolated circularly polarized attosecond pulses by HHG [14].

In this context, the characterization of the time-dependent polarization of the pulse is a key point. The reconstruction of ultrashort pulses has been developed since decades. Nowadays, techniques such as FROG [15], SPIDER [16] or d-scan [17], are well established and allow to measure pulses down to few optical cycles and single-cycle regime [18]–[22]. However, the usual techniques are designed for scalar pulses where pulse polarization is linear and constant on time.

During the last years, different approaches have been proposed to accomplish vector pulse reconstruction in the femtosecond range, e.g., through spectral interferometry in different configurations [23], [24], tomographic reconstruction from measurement of different projections [25], time-resolved ellipsometry [26], some variants [27], [28] based on X-FROG technique [29], nanointerferometric measurement of vector beams [30], or spatial-spectral interferometry [31].

In particular, in dual-channel spectral interferometry method, known as POLLIWOG [21], a linearly polarized known reference pulse interferes with a delayed test (unknown) pulse. By using spectral interferometry analysis [32], the relative phase between two polarization components of the test pulse is extracted. Together with the amplitudes for each polarization projection and the spectral phase of the reference pulse (measured with any scalar temporal pulse reconstruction technique), the time-dependent polarization pulses can be reconstructed. The use of a linear process as interferometry makes it a sensitive and powerful technique, with a non-iterative retrieval algorithm. However, precisely because of this interferometric nature, typical schemes commonly based on standard interferometers such as Mach-Zehnder or Michelson will be very demanding

on stability, in order to preserve the spectral fringes and, more important, to accurately measure the phase difference between the orthogonal components. In fact, the POLLIWOG uses a dual-channel spectrometer to record separately and simultaneously the interferences of the x and y-components, thus preventing shot-to-shot phase fluctuations to affect the polarization component relative phase measurements.

Therefore, it results that, to determine the time-varying polarization state, it is a key point the accurate measurement of the relative amplitude and, primarily, the phase of the polarization component. In this context, to fulfill the stability requirements, our proposal is based on an in-line single-channel spectral interferometry setup, in which the relative phase is directly measured in a crossed intermediate angle projection. The objective of the present work is to implement a robust and reliable technique, not affected by instabilities and noise, and simple in order to be applied to different experimental cases, e.g., PGs that are used for different applications.

Firstly, we present the description of the method and the set-up used for the experimental implementation, accompanied with a first experimental validation of a vector pulse and a study of stability. Secondly, we apply it to the reconstruction of vector pulses obtained from PG technique. All measurements are corroborated by simulations. Finally, we summarize the conclusions.

## 100 II. THE METHOD: IN-LINE SPECTRAL INTERFEROMETRY

101 Our method takes the advantages of using interferometry, a  
102 process characterized by being linear, high sensitivity or a direct  
103 analysis, while avoiding the main drawback, i.e., the instabilities  
104 and alignment requirements. Mostly, spectral interferometry  
105 set-ups are based on interferometers, where the unknown pulse  
106 is combined with the one serving as a reference. These setups  
107 are very sensitive to vibrations and instabilities from the envi-  
108 ronment. To prevent this problem, we use a birefringent element  
109 as a monolithic in-line interferometer, a calcite plate (3 mm of  
110 thickness), with their optical axes parallel to the input and out-  
111 put faces. When an incoming vector pulse passes through the  
112 plate, it is split into the ordinary and extraordinary components,  
113 presenting a delay due to the different refractive indices of the  
114 birefringent material (in our case, 1.8 ps).

115 In previous works, birefringent crystals have already been  
116 used to create stable delayed pulse replicas [33]–[35], which  
117 has been applied to measure the spectral phase of scalar pulses  
118 [34]–[37].

119 After the calcite plate, we use a linear polarizer (LP) to select  
120 different polarization projections of the delayed components  
121 and the corresponding spectra are subsequently acquired by a  
122 spectrometer (AvaSpec 2048-USB1, from Avantes Inc.). Just by  
123 varying the LP orientation, it is possible to measure the spec-  
124 tra from the ordinary and extraordinary components respectively  
125 and the interference between both at an intermediate angle. This  
126 latter spectrum encodes the spectral phase difference among the  
127 ordinary and extraordinary components (once the phase added  
128 by the birefringent plate is subtracted). Therefore, a vector com-  
129 ponent of the pulse is actually acting as a reference for the or-  
130 thogonal one. The use of a *bulk* interferometer means that both

131 components travel through the same physical path and there is  
132 not any other pulse splitting or recombination, thus awarding  
133 the pursued stability to the detection, as well as getting rid of  
134 a precise alignment. Finally, if one of the components is char-  
135 acterized and its spectral phase is known (e.g., by means of a  
136 standard scalar temporal pulse reconstruction technique), it is  
137 possible to reconstruct the vector pulse by applying Fourier-  
138 transform spectral interferometry analysis (FTSI) [32] to the  
139 intermediate projection.

140 The experimental setup and the axes convention are rep-  
141 resented in Fig. 1. Rotation angles for the different elements  
142 will be given with respect to the x-axis and being the observer  
143 looking to the source (positive rotation angle means counter-  
144 clockwise). Firstly, the unknown vector pulse impinges the bire-  
145 fringent plate (calcite 3 mm thickness, 0.5”-side square) that is  
146 located with the extraordinary (fast) axis horizontal (x-axis),  
147 being the y-component of the pulse delayed with respect to  
148 the x-component. The LP can be situated at different angles  
149  $\alpha$ , selecting the corresponding pulse projections,  $S_\alpha$ , that are  
150 detected in the fiber coupled spectrometer.

151 To calibrate in amplitude and phase the system, we create a  
152 calibrating pulse linearly polarized at  $45^\circ$ . This pulse has the  
153 same spectral amplitudes  $A_y(\omega) = A_x(\omega)$  and phases  $\phi_y(\omega) =$   
154  $\phi_x(\omega)$ , so we can obtain the amplitude response of the system  
155 and the relative dispersion of the calcite axes.

156 The horizontal and vertical projections of the LP provide the  
157 information of the amplitude of the x- and y-components, with  
158  $S_{0^\circ} = S_x$  and  $S_{90^\circ} = S_y$  respectively. The intermediate projec-  
159 tion at  $\alpha = 45^\circ$  encodes the relative phase between the orthog-  
160 onal components (x and y):

$$S_{45^\circ} = 1/2S_x + 1/2S_y + \sqrt{S_x S_y} \cos [(\phi_y - \phi_x)_{meas}]. \quad (1)$$

161 This relative phase gathers the pulse phase and the calcite  
162 phase,  $(\phi_y - \phi_x)_{meas} = (\phi_y - \phi_x)_{pulse} + (\phi_y - \phi_x)_{calc}$ , be-  
163 ing the calcite contribution the one that introduces the delay  
164 required to use the FTSI algorithm. In order to remove  
165 the calcite relative dispersion, we used the projection  $S_{45^\circ}$   
166 of the calibrating pulse, for which  $(\phi_y - \phi_x)_{pulse}^{[Calibr]} = 0$  and

$$(\phi_y - \phi_x)_{meas}^{[Calibr]} = (\phi_y - \phi_x)_{calc}. \quad 167$$

168 Regarding the amplitude sensitivity of the fiber coupled  
169 spectrometer to the x and y components, it is corrected with  
170 the  $0^\circ$  and  $90^\circ$  projections of the same calibrating pulse  
171 ( $S_y = S_x$ ). The y-component of the pulse to be measured is  
172 corrected as  $S_y^{[Pulse]} = S_y^{[Pulse]} R_{calibr}$ , where  $R_{calibr}(\omega) =$   
173  $S_y^{[Calibr]}/S_x^{[Calibr]}$  is smoothed and interpolated within the  
174 spectral range of the calibrating pulse.

175 The spectral phase of the component acting as a reference, in  
176 our case the x-component, is measured with a SPIDER device  
177 (any temporal characterization technique is valid). With the LP  
178 set horizontal and a flip mirror, we extract this reference pulse.  
179 Under this configuration, the x-axis dispersion of the calcite  
180 [38] needs to be subtracted (alternatively, the projection of this  
181 reference pulse can be extracted before the calcite).

182 The proposed scheme requires that both the x- and y-  
183 components of the pulse have similar spectral content and  
184 comparable amplitude in order to obtain suitable spectral

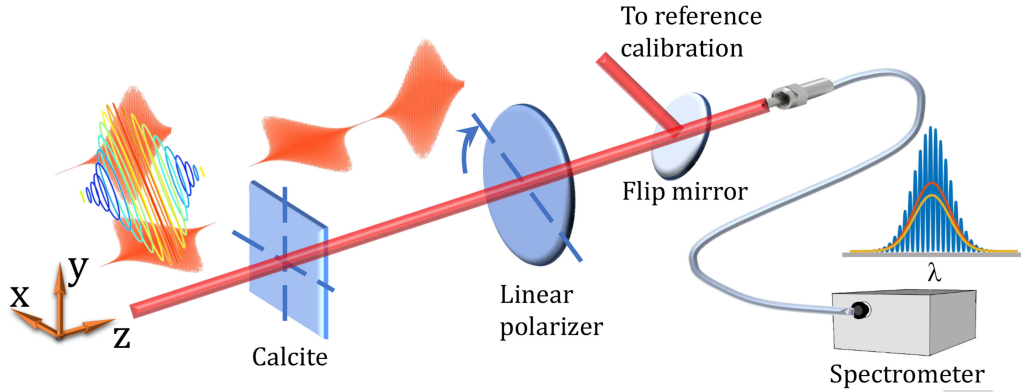


Fig. 1. Schematic of the detection setup for the polarization measurements. The vector pulse passes through a birefringent material (calcite) where the  $x$ - and  $y$ -components are delayed because of the different dispersion. A linear polarizer selects different projections to be measured in the spectrometer (horizontal and vertical projections for the amplitude; intermediate projection to obtain the relative phase of the pulse components). The spectral phase of the horizontal component is measured with an auxiliary device. The system is calibrated using a pulse linearly polarized at  $45^\circ$ .

185 interferences. In the case of having LP polarized at  $0^\circ$  or  $90^\circ$   
 186 (trivial cases), it is possible to rotate the characterization system  
 187 or the pulse e.g.,  $45^\circ$  to optimize the contrast in the detected  
 188 fringes (as we do for the large PG case in the next section  
 189 presenting results). On the other hand, if having different  
 190 spectra at  $0^\circ$  and  $90^\circ$ , the same rotation would merge the spectra  
 191 and lead to fringes in the whole bandwidth.

192 The technique proposed is multi-shot as it uses 3 individual  
 193 projections of the calibrating and unknown pulses, plus the  
 194 reference pulse characterization. The common-path configura-  
 195 tion prevents that shot-to-shot fluctuations of the interferometer  
 196 (due to thermal variations, mechanical vibrations or air fluctua-  
 197 tions) affect the measurement. Laser pulse energy fluctuations  
 198 may affect the retrieval of the relative amplitude of the  $x$ - and  
 199  $y$ -components. In the case of very unstable laser systems, this  
 200 could be circumvented by using dual-channel spectrometers to  
 201 simultaneously measure two projections, together with the re-  
 202 trieval of the relative amplitude between  $S_x$  and  $S_y$  directly  
 203 from the intermediate projection  $S_{45^\circ}$ , in a similar way than in  
 204 [32].

### 205 III. RESULTS: EXPERIMENTS AND SIMULATIONS

#### 206 A. Description of the Experiments and Parameters

207 For the experiments, we have used a CPA Ti:sapphire laser  
 208 (Spitfire, from Spectra Physics) at a repetition rate of 1 kHz,  
 209 emitting 100 fs (FWHM) pulses. To select the different spectral  
 210 projections, we used an achromatic LP (LPVIS050, from Thor-  
 211 labs). For the simulations, we have used the actual experimental  
 212 spectrum of the pulse and then calculated the corresponding pol-  
 213 arization shaping for the different cases. Notice that our pulse  
 214 is centered at 797 nm, while the wave plates employed here are  
 215 designed for 800 nm.

216 From the experimental characterization, we obtain the tem-  
 217 poral amplitude and phase of the vector pulse, from which we  
 218 calculate the polarization state as a function of frequency and  
 219 time, presenting the following magnitudes in the results of Fig. 2,  
 220 4, 5: spectrum (S) and intensity (I) for  $x$  and  $y$  components, el-  
 221 liplicity  $\varepsilon = b/a$  calculated as the minor to major axes ratio,

phase difference  $\delta$  between the  $x$  and  $y$  components, and ori- 222  
 entation of the polarization ellipse (azimuthal angle  $\chi$ ) referred 223  
 to the  $x$ -axis. All vector pulse measurements have been done 224  
 10 times, then calculating the statistical error as the standard 225  
 deviation and representing it in all the retrieved magnitudes as 226  
 a gray shaded area (when not seen it means that it is so small 227  
 that it is not distinguished from the mean value). 228

#### 229 B. Validation and Stability Study

230 The performance of the technique has been tested at known 230  
 cases, trivial and non-trivial. For example, the laser pulses have 231  
 passed through an achromatic half-wave plate, in order to rotate 232  
 their constant polarization direction, which has been verified in 233  
 the measurements. Also, we have characterized the input LP 234  
 pulse passing through a zero-order quarter-wave plate at  $45^\circ$  235  
 creating constant circular polarization. 236

237 Then, a first non-trivial validation consisted in the measure- 237  
 ment of a pulse linearly polarized at  $0^\circ$ , after passing through a 238  
 multiple-order quarter-wave plate (QWPM-800-10-4 from CVI, 239  
 which we label QWPM in the whole manuscript) with the slow 240  
 axis at  $45^\circ$ . This element consisted of a  $652 - \mu\text{m}$  thick quartz 241  
 plate, which introduces a delay of around 20 fs between the fast 242  
 and slow axes for 800 nm. 243

244 We have calibrated it by studying the spectrum transmitted 244  
 when the plate is placed at  $45^\circ$  between two crossed linear pol- 245  
 arizers, using as light source both spectrally broadened pulses and 246  
 incoherent white light. By rotating the last polarizer, clearly the 247  
 plate behaves as a quarter-wave plate around 800 nm, half-wave 248  
 plate at 775 nm and full-wave plate at 825 nm, all at multiple- 249  
 order regime. Thus, when the light passes through the plate, 250  
 oriented at  $45^\circ$ , the state of polarization becomes time-varying 251  
 due to the delay between ordinary and extraordinary compo- 252  
 nents, being not negligible compared to the pulse duration. 253

254 To simulate the vector pulse, we have calculated the disper- 254  
 sion introduced by the QWPM thickness imposing the phase 255  
 difference  $\pi/2$  at 800 nm. The QWPM angle used in the simu- 256  
 lations is  $44^\circ$  (notice that this is compatible with the experi- 257  
 mental error in our rotation mount), being the value for which 258

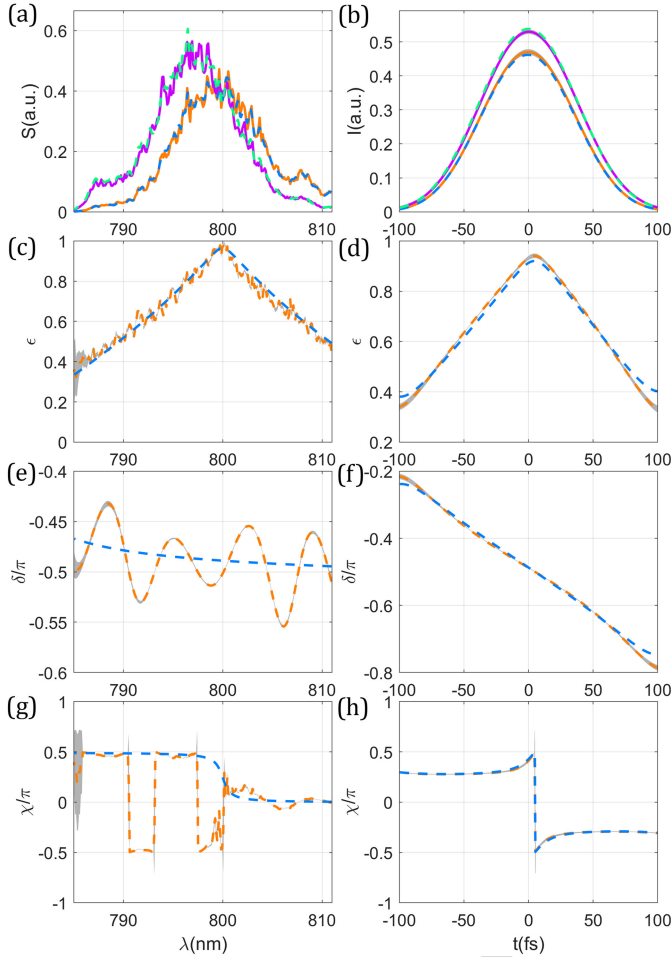


Fig. 2. Polarization results for the case input LP  $0^\circ$ , followed by QWPM slow axis at  $45^\circ$ . Spectral/temporal (a/b) intensity, (c/d) ellipticity  $\varepsilon$ , (e/f) phase difference  $\delta$ , and (g/h) azimuth  $\chi$ , respectively. Plots (a, b), experimental  $x$  (solid red) and  $y$  (solid magenta), simulated  $x$  (dashed blue) and  $y$  (dashed green) components. Plots (c-h), experimental (dashed red), simulated (dashed blue). In all plots the gray shaded area stands for the experimental error.

the simulations match the experimental results ( $\varepsilon$ ,  $\delta$ , and  $\chi$ , simultaneously). Fig. 2 shows the vector pulse reconstruction and simulation results. The spectral amplitude  $x$ ,  $y$  components are laterally shifted (due to the effect of dispersion in a multi-order plate), the spectral ellipticity reaches a maximum ( $\varepsilon \approx 1$ ) with circular polarization (CP) at 800 nm, while the peak at the ellipticity depending on time (close to circular polarization) is shifted to positive times with respect to the peak intensity (we have corroborated that this is because the angle of  $44^\circ$  instead of  $45^\circ$ ).

In order to show the stability of the technique, we used the interference fringes for a pulse with linear polarization at  $45^\circ$ . We did two stability studies, a short-term one with 300 measurements, 1 per second during 5 minutes, and a long-term one with 1500 measurements, 1 each 5 seconds during  $\approx 2$  hours. The fringes were stable and we did not observe the typical mechanical and thermal drift of standard interferometers, as seen in Fig. 3 for the long-term study. Using a fine analysis with the FTSI algorithm, we found the standard deviation of the phase

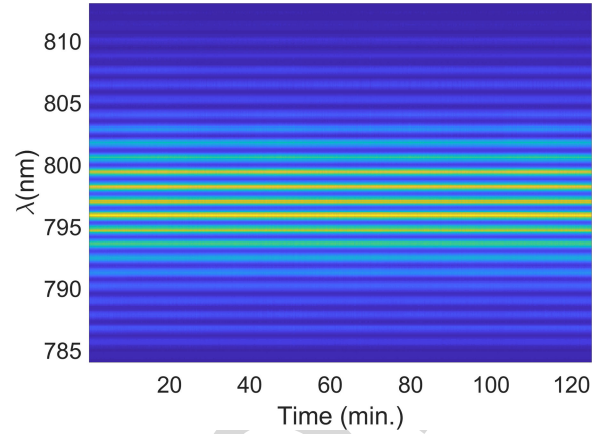


Fig. 3. Spectral interferences recorded with the in-line interferometry setup during 125 minutes used for the long-term stability analysis.

fluctuations to be  $9 \cdot 10^{-4} \cdot 2\pi$  rad and  $4 \cdot 10^{-3} \cdot 2\pi$  rad for the short and long-term studies, respectively. Those values are well below the typical values in standard and non-standard interferometers [39]–[42]. The key point for this stability is the in-line geometry that also confers robustness, accuracy and simplicity to the setup. As said before, this is of paramount importance in the case of the determination of the relative phase between the two polarization components, since it is critical for an accurate calculation of the pulse polarization state. Therefore, the setup can be integrated easily and work at environmental conditions less controlled than the present at a laboratory.

### C. Study of Polarization Gates

Once the performance of the method was tested, we studied the vector pulse coming from PG pulses. As commented previously, that kind of vector pulses are used as one of the main techniques to obtain isolated attosecond pulses [12], [13]. First attempts were performed by using an interferometer in order to delay two orthogonal polarization components of an incoming linearly polarized pulse, in order to obtain circular polarization at the center of the outgoing pulse, and linear polarization at the edges [10]. A zero-order quarter-wave plate (QWP0) aligned at  $45^\circ$  converted the linear polarization into circular and the circular polarization into linear, obtaining a vector pulse exhibiting linear polarization only in its center, while ellipticity rises at the edges. A simpler and more compact version consists in using a combination of a multiple-order (QWPM) and a zero-order (QWP0) quarter-wave plate [10], [11]. The element QWPM is the same than before, whereas the element QWP0 is a zero-order quartz plate designed for operation at 800 nm (QWP0-800-08-4-R10 from CVI). The input pulse has LP at  $0^\circ$ , then the QWPM is orientated with the slow axis at  $45^\circ$ . After that, the QWP0 is situated with the fast axis at  $90^\circ$  to create the so-called narrow PG (results in Fig. 4), characterized by having linear polarization at the center of the pulse and circular polarization at the pulse edges.

After the QWPM, the pulse is that presented in Fig. 2, with CP at the maximum intensity, with ellipticity decreasing at the

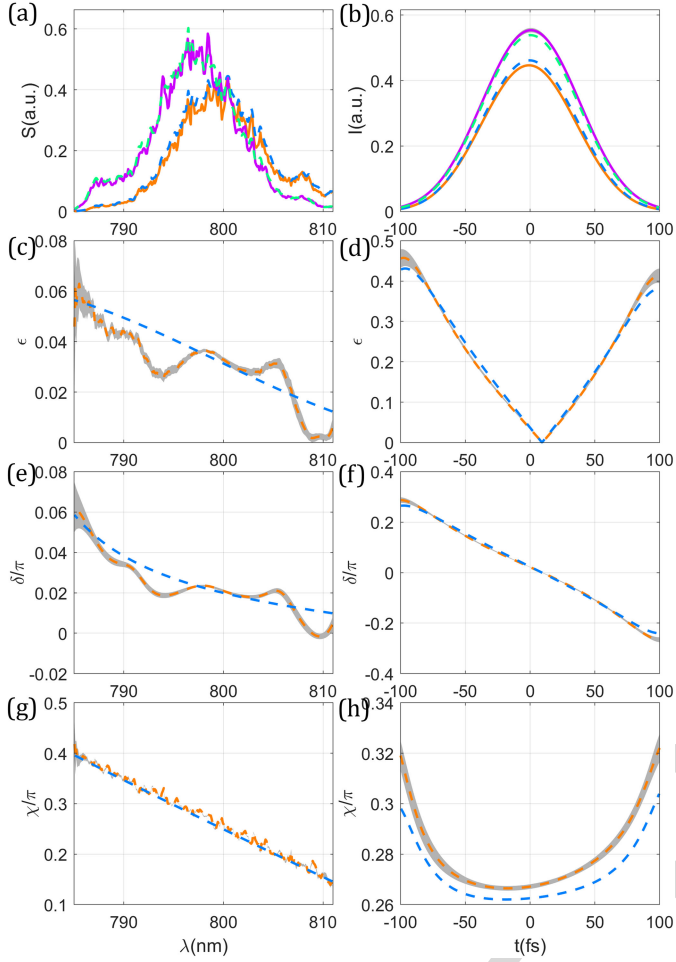


Fig. 4. Polarization results for the narrow PG (input LP  $0^\circ$ , followed by QWPM slow axis at  $45^\circ$ , and QWP0 fast axis at  $90^\circ$ ). Spectral/temporal (a/b) intensity, (c/d) ellipticity  $\epsilon$ , (e/f) phase difference  $\delta$ , and (g/h) azimuth  $\chi$ , respectively. Plots (a, b), experimental  $x$  (solid red) and  $y$  (solid magenta), simulated  $x$  (dashed blue) and  $y$  (dashed green) components. Plots (c-h), experimental (dashed red), simulated (dashed blue). In all plots the gray shaded area stands for the experimental error.

edges of the pulse (ideally reaching LP if the delay introduced between the QWPM components is high enough compared to the pulse duration, which is not our case). If then QWP0 is at  $90^\circ$  (with respect to the  $x$ -axis) the CP of the maximum is converted to LP and the ellipticity at the edges now increases (in the limit ideally being CP), thus creating a narrow PG with an effective LP region shorter than the initial pulse duration. The azimuth is almost constant at  $45^\circ$  in the temporal domain, and the direction of rotation is seen to change at the maximum intensity (with the sign of  $\delta$ ).

In the so-called large PG, the pulse is characterized because the temporal ellipticity is zero (LP) while the azimuth of the LP is rotating along the pulse duration. The fast axes of the QWP0 and QWPM wave plates are aligned at  $45^\circ$  with respect to the input LP. Under this configuration, the output pulse would be almost LP at  $90^\circ$ . To avoid this, we rotate the system  $45^\circ$ , where the initial pulse passes through a LP at  $45^\circ$  (polarizing cube), then the QWPM and the QWP0 wave plates are orientated with

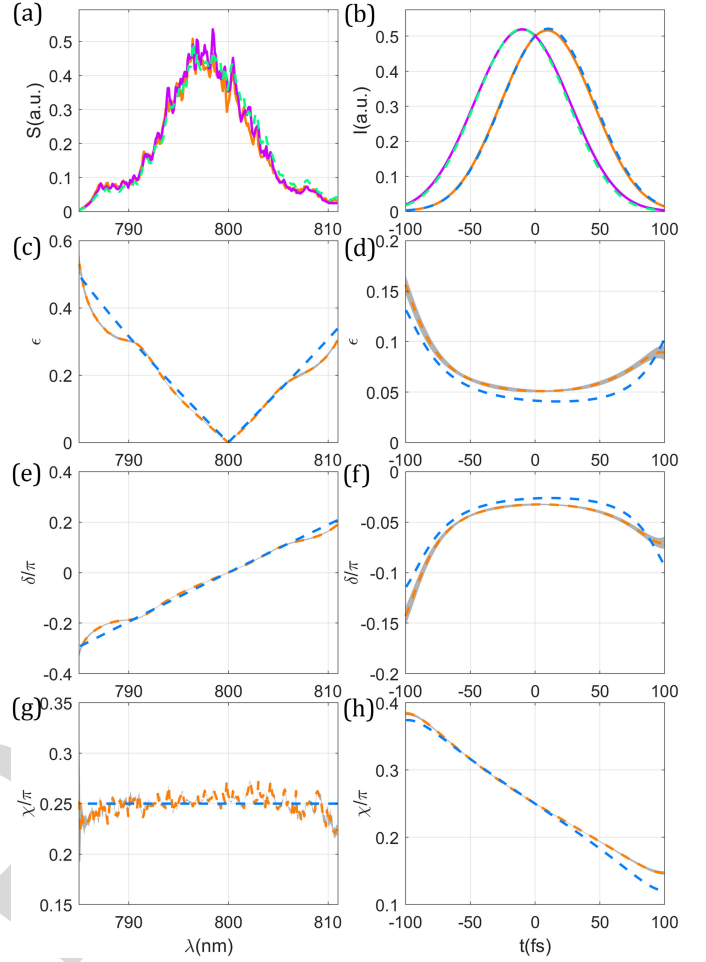


Fig. 5. Polarization results for the large PG (input LP  $45^\circ$ , followed by QWPM fast axis at  $0^\circ$ , and QWP0 fast axis at  $90^\circ$ ). Spectral/temporal (a/b) intensity, (c/d) ellipticity  $\epsilon$ , (e/f) phase difference  $\delta$ , and (g/h) azimuth  $\chi$ , respectively. Plots (a, b), experimental  $x$  (solid red) and  $y$  (solid magenta), simulated  $x$  (dashed blue) and  $y$  (dashed green) components. Plots (c-h), experimental (dashed red), simulated (dashed blue). In all plots the gray shaded area stands for the experimental error.

their fast axes at  $90^\circ$  (results in Fig. 5). The temporal ellipticity is kept almost constant below 0.1, LP as expected, while the polarization azimuth evolves on time (from  $90^\circ$  to  $0^\circ$ , being  $45^\circ$  at the center of the pulse).

A full experimental characterization of the PGs [43] is important to predict, optimize and understand the applications of those pulses [44], considering that the real pulse may differ from the expected one e.g., due to the use of non-ideal retarders or non-Gaussian pulse spectrum.

#### IV. CONCLUSION

In sum, we have presented a simple and compact in-line, single-channel device to reconstruct vector pulses. The capabilities of the technique have been demonstrated with different cases of known pulses, being the results corroborated by the simulations. The small statistical error in the retrievals shows a good performance in the measurements, which is related to the

349 excellent stability of the compact *bulk* interferometer. We have  
 350 used it to fully characterize PGs of interest for their associated  
 351 applications. The robustness of the setup makes it suitable in  
 352 more demanding future experimental situations, e.g., after non-  
 353 linear propagation, out laboratory conditions or to characterize  
 354 vector beams that are nowadays used in many applications.

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