# Comparison Between the Dynamic Performance of Double- and Single-Gate AlInAs/InGaAs HEMTs

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Abstract—The static and dynamic behavior of InAlAs/InGaAs double-gate high-electron mobility transistors (DG-HEMTs) is studied by means of an ensemble 2-D Monte Carlo simulator. The model allows us to satisfactorily reproduce the experimental performance of this novel device and to go deeply into its physical behavior. A complete comparison between DG and similar standard HEMTs has been performed, and devices with different gate lengths have been analyzed in order to check the attenuation of short-channel effects expected in the DG-structures. We have confirmed that, for very small gate lengths, short-channel effects are less significant in the DG-HEMTs, leading to a better intrinsic dynamic performance. Moreover, the higher values of the transconductance over drain conductance ratio  $g_m/g_d$  and, especially, the lower gate resistance  $R_g$  also provide a significant improvement of the extrinsic  $f_{max}$ .

*Index Terms*—Double-gate high-electron mobility transistor (DG-HEMT), dynamic behavior, Monte Carlo (MC) simulations.

## I. INTRODUCTION

nP-BASED high-electron mobility transistors (HEMTs) have proved to exhibit an excellent performance for applications in the microwave and millimeter-wave frequency ranges [1]. To further improve the frequency operation of these devices, their gate length  $L_q$  has been reduced down to the technological limit. In this way, a cutoff frequency  $f_t$  of 562 GHz and a maximum oscillation frequency  $f_{\text{max}}$  of 330 GHz have been obtained in a T-gate InAlAs/InGaAs pseudomorphic HEMT by reducing  $L_a$  down to 25 nm [2]. The reduction of the source and drain parasitic resistances by using a multilayer cap technology in a 30-nm-gate-length structure allowed us to reach an  $f_{\rm max}$  of 400 GHz, together with a simultaneously high  $f_t$  of 547 GHz [3]. However, very small values of  $L_g$  involve the so-called short-channel effects (the gate capacitance does not scale with  $L_q$  anymore, and the transconductance  $g_m$  and the output conductance  $g_d$  are deteriorated), which limit the

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 Mag
 E-Beam
 Det
 FWD
 500 nm

Fig. 1. SEM image of a 100-nm-gate DG-HEMT fabricated in the IEMN (Lille, France).

microwave performance of the HEMTs. To avoid these effects, a vertical scaling of the layer structure must go along with the reduction of the gate length in order to keep a high aspect ratio  $L_g/a$ , where a is the distance between the gate electrode and the 2-D channel electron gas. This scaling rule is limited by the emergence of a leakage current through the Schottky barrier at the gate; thus, this distance cannot be reduced to less than 8–10 nm. Then,  $f_t$  cannot scale up anymore with  $L_g$ . The device aspect ratio is consequently considered as the fundamental limit of HEMTs.

To keep on improving the frequency performance of these transistors (especially regarding  $f_{\text{max}}$ ), alternative solutions based on an evolution of the standard HEMT design have been considered. Thus, the double-gate HEMT (DG-HEMT), which is a HEMT with two gates placed on each side of the conducting InGaAs channel (see Fig. 1), has been recently developed [4]–[6]. Even if this idea was conceived some time ago for Si-devices [7]–[9], the authors in [4]–[6] show, for the first time to our knowledge, the fabrication of DG-transistors on III-V materials. In those previous works [4]-[6], we have reported the fabrication of a 100-nm T-gate DG-HEMT, which exhibits a very high extrinsic  $g_m$  and a good pinchoff behavior (lower  $g_d$ ) as compared with the conventional single-gate (SG)-HEMT. This happens since the DG geometry can provide a better charge control and counteracts the effect of carrier injection into the buffer (since no buffer is used in the structure).

In order to better understand the intrinsic performance and to provide a theoretical model for this brand-new device, we present a complete study of  $In_{0.52}Al_{0.48}As/In_{0.53}Ga_{0.47}As$ DG-HEMT structures carried out by means of a semiclassical 2-D ensemble Monte Carlo (MC) simulator [10]–[12]. Our model allows us to satisfactorily reproduce the static and dynamic performances of the experimental DG-HEMT presented in [5] and [6], thus confirming its validity for the simulation of DG-devices. It also provides a fully microscopic interpretation of the differences in the static and dynamic performances of the DG-HEMT, in comparison with a similar standard SG-HEMT. In addition, devices with different  $L_g$  are simulated to verify the expected attenuation of short-channel effects in DG-devices.

This paper is organized as follows. In Section II, the physical model employed in the analysis is described. Later, the comparison between the experimental and simulated 100-nm DG- and SG-HEMTs, both of static characteristics and small signal equivalent circuit (SSEC) parameters, is presented in Section III in order to validate our model. In Section IV, the MC results for the 100- and 50-nm-gate-length devices are shown. Finally, in Section V, the most important conclusion of this paper is drawn.

#### II. PHYSICAL MODEL

For the calculations, we make use of a semiclassical ensemble MC simulator, self-consistently coupled with a 2-D Poisson solver whose validity has been previously checked for conventional HEMTs [10]–[12]. The model takes into account important physical effects, as the influence of degeneracy in the electron accumulation appearing in the channel by using the rejection technique [10]. The schemes of the DG- and SG-device topologies used in the simulations are shown in Fig. 2. They are a recessed  $In_{0.52}Al_{0.48}As/In_{0.53}Ga_{0.47}As$ DG-HEMT and the corresponding standard SG-HEMT. The layer structure is similar to that of the 100-nm-gate fabricated transistors [5], [6] to establish a correspondence with the experimental measurements.

Our MC algorithm allows us to analyze transistors with different gate lengths (the experimental one, where  $L_g = 100$  nm, and the shorter ones, where  $L_g = 25$  and 50 nm) to check the attenuation of short-channel effects expected for DG-devices with respect to standard SG-HEMTs. In order to provoke important short-channel effects and thus facilitate the study, the scaling down of the vertical dimensions is not performed when reducing  $L_g$  from 100 to 50 and 25 nm (the vertical thicknesses of the different layers are kept the same).

With regard to the dynamic behavior, the same intrinsic SSEC is considered for both types of devices [10]–[13]. This is correct as long as the DG-HEMT works in a common mode, i.e., the potential applied at both gate electrodes ( $V_{\rm GS1} = V_{\rm GS2} = V_{\rm GS}$ ) is identical. The SSEC is calculated, taking as a basis the Y-parameters, obtained by using the typical MC technique [13]. After that, the intrinsic cutoff frequency  $f_C$  is calculated as  $g_m/2\pi C_{\rm gs}$ . Finally, having established a correspondence between measurements and MC results, the experimental parasitic elements can be taken into account in the SSEC for the correct calculation of the extrinsic  $f_t$  and  $f_{\rm max}$ .



Fig. 2. Schematic drawing of the simulated SG- and DG-HEMTs.

# III. COMPARISON BETWEEN EXPERIMENTAL AND MC RESULTS

In order to carry out the comparison of the measured results (extrinsic) with those obtained from the simulation (intrinsic), it is necessary to include, in a postprocessing stage, the parasitic elements that are not considered in the intrinsic MC model. Thus, drain  $(R_D^{\text{met}})$  and source  $(R_S^{\text{met}})$  parasitic resistances associated with metallizations have been incorporated into the original MC results, with the best fit being obtained for  $R_D^{\text{met}} = 0.15 \ \Omega \cdot \text{mm}$  and  $R_S^{\text{met}} = 0.10 \ \Omega \cdot \text{mm}$ , which are found to coincide in both devices. By separately adjusting the surface charge at the cap layer and at the bottom of the recess ( $6.2 \times 10^{16} \text{ and } 4.3 \times 10^{16} \text{ m}^{-2}$ , respectively), the static characteristics of the experimental 100-nm-gate DG- and SG-HEMTs [5] can be very nicely reproduced by our MC simulator, as shown in Fig. 3.

Regarding the dynamic behavior of the HEMTs, Fig. 4 shows the comparison between the experimental and the MC values of the main intrinsic SSEC parameters ( $g_m$ ,  $g_d$ ,  $C_{gs}$ , and  $C_{gd}$ ) for the 100-nm-gate DG- and SG-HEMTs, where  $V_{DS} = 0.5$  V. For the calculation of the MC results, in order to extract the actual intrinsic SSEC, the access resistances corresponding to the ohmic regions near the source and drain electrodes  $R_S^{acc}$  and  $R_D^{acc}$ , respectively, are removed from the raw simulated values. The values for these parameters are extracted from the experimental measurements (in the 100-nmgate devices) of the total parasitic resistances  $R_S^{exp}$  and  $R_D^{exp}$ by subtracting the resistances of metallizations, providing the



Fig. 3. Comparison of the extrinsic  $I_D - V_{\rm DS}$  curves measured in fabricated 100-nm-gate (a) DG- and (b) SG-HEMTs with those obtained from the MC simulation of similar devices. The gate voltage of the top curves is  $V_{\rm GS} = 0.0$  V, and the step of the gate bias is  $\Delta V_{\rm GS} = 0.1$  V for both sets of curves. (c) Corresponding  $I_D - V_{\rm GS}$  curves for  $V_{\rm DS} = 0.5$  V.

following:  $R_S^{\rm acc} = R_S^{\rm exp} - R_S^{\rm met} = 0.08 \ \Omega \cdot \text{mm}$  and  $R_D^{\rm acc} = R_D^{\rm exp} - R_D^{\rm met} = 0.11 \ \Omega \cdot \text{mm}$  in the DG-HEMT and  $R_S^{\rm acc} = 0.23 \ \Omega \cdot \text{mm}$  and  $R_D^{\rm acc} = 0.22 \ \Omega \cdot \text{mm}$  in the SG-HEMT. The same values are used for the 50-nm-gate devices. Note that the access resistances are lower for the DG-HEMT than for the SG-device due to the higher carrier concentration.

In addition, it is necessary to include the so-called "external" geometric capacitances between the contact accesses  $C_{\rm gs}^{\rm ext}$  and  $C_{\rm gd}^{\rm ext}$  (extracted from the comparison of the results of the simulations at  $I_D = 0$  with the experimental measurements, as explained in [10] and [11]). The values obtained for the 100-nm-gate devices (which will also be used for the 50-nm ones since the same layout is considered) are the following:  $C_{\rm gs}^{\rm ext} = 280$  fF/mm and  $C_{\rm gd}^{\rm ext} = 255$  fF/mm for the DG-HEMT and  $C_{\rm gs}^{\rm ext} = 210$  fF/mm and  $C_{\rm gd}^{\rm ext} = 152$  fF/mm for the SG-HEMT.

In general, we find a good agreement between the experimental and the MC results for  $g_m$  and  $C_{\rm gd}$  for both DG- and

SG-transistors. The discrepancy in the values of  $g_d$  for high  $V_{GS}$ can be attributed to the experimental frequency dispersion due to traps and other layer defects which are not included in the MC model. It seems that, in a dynamic operation, the devices are more resistive, so that the stationary bias point, which is in the saturated region of the I-V curves, may be shifted to the linear part of the characteristics (providing the increase of  $g_d$  for high  $V_{\text{GS}}$ ). Indeed, the static value of  $g_d$  is well reproduced by the simulations, as confirmed by the satisfactory agreement of the I-V curves [Fig. 3(a) and (b)]. On the other hand, MC simulations somewhat underestimate the values of  $C_{\rm gs}$ , mainly in the DG-HEMT (even if the agreement can be considered reasonable up to  $V_{\rm GS} = -0.2$  V). The cause for this discrepancy can again be the not-considered layer defects. We remark that experimental Hall measurements show a degradation of the mobility in the channel of the DG-HEMTs. This fact, together with the common overestimation of the electron velocity given by the ideal MC model [10]-[12], means that the electron concentration in the simulations fitting the experimental values of  $I_d$  and  $g_m$  is probably lower than the real one (mainly in the DG-HEMT), which can also lead to lower values of  $C_{\rm gs}$ .

#### IV. MC COMPARISON BETWEEN DG- AND SG-HEMTS

The simulated extrinsic output characteristics for 100- and 50-nm-gate DG (where  $V_{\rm GS1} = V_{\rm GS2} = V_{\rm GS}$ ) and SG-HEMTs with a device width of  $W = 100 \ \mu m$  are shown in Fig. 5. The drain current provided by the DG-HEMTs is about twice that given by the SG-transistors (as shown in Fig. 3). This occurs because the electron concentration in the DG-HEMT channel is significantly higher than in the conventional HEMT (for both values of  $L_g$ ) due to the presence of two charge-accumulation regions. This can be appreciated in Fig. 6, where the electron density profile along the vertical direction under the gate of the 100-nm DG- and SG-HEMTs is presented ( $V_{\rm DS} = 0.5$  V and  $V_{\rm GS} = -0.1$  V).

The immunity to short-channel effects in the static characteristics achieved with the DG-architecture is confirmed by the results shown in Fig. 7, which reports the behavior of the threshold voltage ( $V_T$ , calculated by extrapolating to zero current the  $\sqrt{I_D}$  versus  $V_{\rm GS}$  plot) when shortening  $L_g$ . In Fig. 7(a), it is observed that the  $V_T$  roll-off is less pronounced in the DG-structure than in the SG-one. Drain-induced barrier lowering (DIBL, calculated as the difference between the values of  $V_T$  for  $V_{\rm DS} = 1.0$  and 0.5 V) is also reduced in the DG-device, as shown in Fig. 7(b). Regarding subthreshold swing, the value experimentally found in the DG-structure (75 mV/dec) is much lower than in the SG-HEMT (125 mV/dec) for the 100-nmgate devices. This parameter cannot reliably be calculated with MC simulations because of the extremely low current level.

With regard to the dynamic behavior of the transistors, Fig. 8 shows that the MC values of  $g_m$  are notably higher in the DG than in the conventional HEMT due to the approximately double charge in the channel. When decreasing  $L_g$ , an increase of  $g_m$  would be expected, but this does not happen. This is due to the nonoptimized layer structure of the 50-nm-gate devices.



Fig. 4. Experimental and MC values of (a) and (c)  $g_m$  and  $g_d$ , and (b) and (d)  $C_{gs}$  and  $C_{gd}$  versus  $V_{GS}$  for the 100-nm-gate (a) and (b) DG- and (c) and (d) SG-HEMTs.  $V_{DS} = 0.5$  V.



Fig. 5. MC extrinsic output characteristics for the (a) 100-nm- and (b) 50-nmgate DG- and SG-HEMTs that are shown in Fig. 2. The gate voltage for the top curves is  $V_{\rm GS} = 0.1$  V, and the step of the gate bias is  $\Delta V_{\rm GS} = 0.1$  V.

This short-channel effect is more evident in the SG-HEMT, for which  $g_m$  decreases when reducing  $L_g$ , while in the case of the DG-HEMT, it remains approximately the same, which is a clear evidence of the expected attenuation of short-channel effects in DG-HEMTs. This result constitutes a remarkable proof of the



Fig. 6. Transversal profile of electron concentration under the gate for the simulated 100-nm DG- and SG-HEMTs. The top gate is at the left, and the bottom gate (or the substrate) is at the right side of the graph.  $V_{\rm DS} = 0.5$  V and  $V_{\rm GS} = -0.1$  V.

improved charge control achieved by the presence of two gates. Another improvement introduced by the new device geometry is the reduction of  $g_d$ , which is shown in Fig. 8(b) (at least up to  $V_{\rm GS} = -0.1$  V, where the DG-HEMTs approach the linear region and  $g_d$  sharply increases), due to the absence of buffer in those structures. An increase in  $g_d$  is appreciated in both types of devices when reducing  $L_g$  due to the enhanced shortchannel effects. It is noticeable that the combined effects of a higher  $g_m$  and a lower  $g_d$  induce an extremely high intrinsic unloaded voltage gain  $g_m/g_d$  in the DG-HEMTs, which is more than three times than that obtained for the SG-HEMTs. This fact, as will be shown later, leads to an improved value of  $f_{\rm max}$ .



Fig. 7. (a)  $V_T$  for  $V_{\rm DS} = 0.5$  V and (b) DIBL, calculated as the difference between  $V_T$  for  $V_{\rm DS} = 1.0$  V and 0.5 V, for the simulated SG- and DG-HEMTs as a function of  $L_g$ .



Fig. 8. MC values of (a)  $g_m$  and (b)  $g_d$  versus  $V_{\rm GS}$  for the 50- and 100-nm-gate DG- and SG-HEMTs.  $V_{\rm DS}=0.5$  V.

The MC values of the gate-to-source  $C_{\rm gs}$  and gate-todrain  $C_{\rm gd}$  capacitances for the different transistors are shown in Fig. 9. It can be observed that the values of both  $C_{\rm gs}$  and



-0.2

0.0

0.2

-0.4

=50 nm 100 nm

DG

1200

1000

800

600

400

200

0

500

400

300

200

100

-0.8

-0.6

Cgd (fF/mm)

C<sub>gs</sub> (fF/mm)

Fig. 9. MC values of (a)  $C_{\rm gs}$  and (b)  $C_{\rm gd}$  versus  $V_{\rm GS}$  for the 50- and 100-nm-gate DG- and SG-HEMTs.  $V_{\rm DS}=0.5$  V.



Fig. 10. MC values of  $f_C$  versus  $V_{\rm GS}$  for the 50- and 100-nm-gate DG- and SG-HEMTs.  $V_{\rm DS}=0.5$  V.

 $C_{\rm gd}$  are almost twice in the DG-HEMT as compared to the conventional HEMT due to the presence of two gates and two regions of electron accumulation in the channel (Fig. 6). The reduction of the gate length affects the capacitances of both types of devices in a similar way:  $C_{\rm gs}$  decreases (even if its reduction is not proportional to  $L_g$  due to short-channel effects) and  $C_{\rm gd}$  remains almost the same (the intrinsic contribution is almost negligible with respect to the "external" geometric capacitance).

The MC intrinsic cutoff frequency  $f_C$  of the simulated devices is shown in Fig. 10 as a function of  $V_{\rm GS}$  for  $V_{\rm DS} = 0.5$  V. The significant increase of  $g_m$  in the DG with respect to the SG-HEMTs is compensated by the higher values of  $C_{\rm gs}$ , thus surprisingly providing lower values of  $f_C$  for the 100-nm-gate DG with respect to the SG-devices. Evidently, the value

(a)

(b)

0.4

of  $C_{gs}^{ext}$  has a strong influence on these results for  $f_C$ , and it must be minimized, as much as possible, in the design of the experimental devices. This qualitative behavior is in good agreement with the experimental measurements, even if the simulated values of  $f_C$  are somewhat higher (MC simulations predict a maximum of 401 and 387 GHz for the SG- and DG-HEMTs, respectively, whereas the measurements reach only 369 and 320 GHz, respectively), which can be attributed to the overestimation of the electron mobility in the channel and the lower values of  $C_{gs}$  [Fig. 4(b)]. In addition, the difference between the simulated values of  $f_C$  for SG- and DG-devices is reduced, as compared to the measurements due to the degradation of the mobility in the DG-HEMT. It is also important to remark that, when reducing  $L_g$ , the maximum  $f_C$  significantly increases in the DG-device, becoming higher than the SG-one, where a small improvement of  $f_C$  is found due to the more pronounced increase of short-channel effects and the consequent deterioration of  $g_m$ . In spite of the slight discrepancy between experimental and MC results, the simulations provide very useful information about the comparison of the purely intrinsic performance of DG- and SG-HEMTs. In fact, our simulations show that, as long as the devices have a sufficient aspect ratio (thus avoiding important short-channel effects, as in the case of 100-nm devices), the DG architecture does not provide any significant improvement with respect to the SG-HEMTs in terms of  $f_C$ , but when short-channel effects are more pronounced, the improvement obtained with DGstructures can be significant (as in the case of 50-nm-gate devices).

In order to complete the comparison of the DG- and SG-HEMT dynamic behavior, we have obtained the values of their extrinsic cutoff frequencies  $f_{\text{max}}$  and  $f_t$ , defined as the values for which the unilateral gain U and the short-circuit current gain  $H_{21}$  is equal to one, respectively. In contrast to  $f_C$ , only regarding the intrinsic performance of the devices (and not being influenced by the values of  $g_d$  or  $C_{\rm gd}$ ),  $f_{\rm max}$ and  $f_t$  account for the device parasitics [5], [6] and provide more practical information about the dynamic performances of the devices for analog and digital applications, respectively. For example, the fact that the DG-HEMT benefits from two gates in parallel is of great importance, thus reducing its gate resistance to nearly half that of the SG-HEMT ( $R_G = 17$  and 38  $\Omega/\text{mm}$ , respectively). In addition, as shown before, source and drain access resistances  $(R_S^{\rm acc} \mbox{ and } R_D^{\rm acc})$  are much lower in the DG-HEMTs. The MC values of  $f_{\text{max}}$  and  $f_t$  as a function of the gate bias are shown in Fig. 11 (the inset shows the typical frequency behavior of U and  $|H_{21}|^2$ ), and their maximum values are presented in Table I.  $f_t$  is calculated by extrapolating the low-frequency behavior of  $H_{21}$ , while  $f_{\text{max}}$  is the exact value for which U = 1 (thus correctly considering the frequency dependence of U, as explained in [12]).

In Fig. 11(a), it is observed that, in the 100-nm-gate DG-HEMT, the values taken by  $f_{\text{max}}$  are higher than in the SG-structure. More exactly, the simulations show a significant improvement (around 30%) in the maximum values of  $f_{\text{max}}$ : 287 GHz for the DG-HEMT and 226 GHz for the SG-HEMT (in good agreement with the results of the measurements, which are 288 and 220 GHz, respectively). Regarding  $f_t$  [Fig. 10(b)],



Fig. 11. MC values of (a)  $f_{\rm max}$  and (b)  $f_t$  versus  $V_{\rm GS}$  for the 50- and 100-nm-gate DG- and SG-HEMTs.  $V_{\rm DS} = 0.5$  V. The inset shows U and  $|H_{21}|^2$  versus frequency for the 100-nm devices for a gate bias corresponding to the maximum  $f_{\rm max}$ .

TABLE IMAXIMUM VALUES OF  $f_{max}$  and  $f_t$  for the Different DevicesObtained With MC Simulations.  $V_{DS} = 0.5$  V

fmax (GHz)	Lg=100 nm	$L_g=50 \text{ nm}$	ft (GHz)	$L_g=100 \text{ nm}$	$L_g=50 \text{ nm}$
SG-HEMT	226	218	SG-HEMT	209	215
DG-HEMT	287	286	DG-HEMT	214	258

the simulations and the experiments show similar values for the 100-nm-gate DG- and SG-devices (around 200 GHz). When reducing  $L_g$  to 50 nm,  $f_{\text{max}}$  is about the same in both types of devices due to the important short-channel effects provoked by the reduced aspect ratio. On the contrary, the value of  $f_t$  in the DG-HEMT increases with respect to the 100-nm-gate device (reaching 258 GHz, which is an important 20% increase), while it is not improved in the SG-HEMT (the increase of  $f_C$  is higher in the DG-HEMT; Fig. 10). As shown in Fig. 11, the improvement of  $f_{\text{max}}$  in the DG-architecture is greater than that of  $f_t$  due to a reduced value of  $R_g$  and  $g_d$ , which have a significant influence on  $f_{\text{max}}$ , without much affecting the value of  $f_t$ . For this same reason, the strong degradation of  $g_d$  when decreasing the gate length prevents the increase of  $f_{\text{max}}$ , while  $f_t$  is improved.

These results show that, even if the purely intrinsic behavior of DG-devices is not much improved with respect to the standard SG-architecture when devices have a sufficiently high aspect ratio, DG-HEMTs demonstrate a noticeably superior extrinsic frequency performance and a higher immunity to short-channel effects due to the reduced parasitic resistances and lower drain conductance.

## V. CONCLUSION

We have presented an MC-based study of DG-HEMTs, comparing their static and dynamic performances with standard SG-devices. The good agreement between the experimental and simulated results is the starting point for the comparison of the intrinsic and extrinsic behaviors of both types of devices, without being affected by the technological problems that can hinder an experimental comparison (as it happens with the degradation of the electron mobility in the DG-HEMT). The simulations of the 50- and 25-nm-gate devices with low aspect ratio clearly demonstrate the expected improved immunity to short-channel effects in the static characteristics of DG-HEMTs with respect to SG-structures (in terms of the behavior of  $V_T$  roll-off, DIBL, and subthreshold swing). However, the improvement of the purely intrinsic dynamic behavior of the DG-HEMTs over the standard devices does not come out in well-designed devices since the increase of  $g_m$  is partially compensated by higher values of  $C_{gs}$ . However, the differences are more evident when comparing the extrinsic  $f_{\text{max}}$ . The higher  $g_m/g_d$ , together with lower  $R_g$  and source and drain access resistances, leads to significantly higher values of  $f_{\max}$  in the DG-HEMTs.

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