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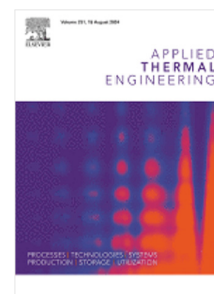
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# Promising research trends for solar parabolic dish collectors

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## Abstract

Concentrated Solar Power (CSP) systems are among the most promising renewable energy technologies in the energy transition scenario. Parabolic dish collectors (PDCs) mainly gather solar power and concentrate it onto a receiver located at the focus of a reflecting paraboloid. They reach the highest concentration factor among CSP configurations. Thus, temperatures even above 1000°C can be achieved. Traditionally, these systems were devoted to producing electricity through a thermodynamic cycle running with a fluid heated up at the receiver working either alone or integrated within micro-cogeneration energy systems or smart grids. However, provided the high temperature these systems can achieve, a wide range of innovative applications related to thermal energy production are emerging. Combined heat and power, water desalination, synthetic fuel, hydrogen production, or thermal energy storage purposes constitute some examples of those new challenging uses. Besides aiming to decentralize electric energy production, parabolic dish collectors can compete or be hybridized with photovoltaic systems to fulfill distributed energy production demand. This work addresses theoretical and practical issues concerning the above novel and challenging applications, filling a gap in the current literature on the prospects for solar parabolic dish collectors.

*Keywords:* Concentrated solar power, Parabolic dish collector, High temperature applications, Hybridization, Thermal energy, Distributed energy, Storage configurations.

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40 **Nomenclature**

CAES	Compressed Air Energy Storage
CFD	Computational Fluid Dynamics
CHP	Combined Heat and Power
CSP	Concentrated Solar Power
DNI	Direct Normal Irradiance
DSDC	Discretized Solar Dish Collector
FIT	Feed-in Tariff
HTF	Heat Transfer Fluid
HRES	Hybrid Renewable Energy System
LAES	Liquid Air Energy Storage
LCA	Life Cycle Assessment
LCoE	Levelized Cost of Electricity
LCoH <sub>2</sub>	Levelized Cost of Hydrogen
MCRT	Monte-Carlo Ray Tracer
MGT	Micro-gas Turbine
MOP	Multi-Objective Optimization Problem
PF	Pareto Front
PCM	Phase-change materials
PDC	Parabolic Dish Collector
PV	Photovoltaic
TES	Thermal Energy Storage
TCES	Thermo-chemical Energy Storage
TRL	Technology Readiness Level

41

## 1. Introduction: Current status, challenges, and future directions of the technology

Parabolic dishes (PDCs) are generally regarded to be the most efficient CSP systems due to their largest concentration factor [1000-4000] when compared with other collectors such as parabolic troughs or linear Fresnel collectors [60-80], or solar towers [300-1000] [1, 2, 3]. In contrast to other kinds of solar collectors, parabolic dishes can be used for small-scale generation, for instance, for distributed applications to produce a modest amount of power or heat [0.01-0.4] MW in the vicinity of the consumption site [4], sometimes making use of low-cost solutions [5]. Nevertheless, PDCs have a peculiarity that makes them to play a particular role: their modularity. Although standing-alone dishes can produce power on a kW scale with an interesting potential market [6], their arrangement allows for incremental capacity addition. This means the potential customer can experiment with the technology without a large initial investment [5, 7]. In that case, the essential ingredient to be competitive is the levelized cost of generated electricity (LCoE) in the frame of other renewable technologies.

As with other CSP plants, parabolic dishes can produce electric power, heat for industrial applications or others, and combined heat and power (CHP). But unlike parabolic troughs and central tower plants, the most developed technologies at a commercial level, PDC has specific applications and markets.

PDCs can be coupled through the receiver to a thermodynamic cycle and a subsequent electric generator to produce electric power. From a historical viewpoint, Stirling engines were the first thermal engines employed [8, 7]. Other options are Rankine [9] or Brayton [10] cycles. In the last case, the most promising nowadays, micro gas turbines [11], are modified so that the solar receiver is placed between the recuperator and the combustion chamber. The heat transfer fluid (HTF) flowing through the solar receiver (usually air) is heated by forced convection and then goes to the combustor, where it can be additionally heated up if necessary (hybridization concept). Thus, an approximately fixed turbine inlet temperature and a dispatchable constant power output are ensured.

On the other side, it could be stated that high-temperature processes account for a large share of the whole world's energy requirements [12]. Almost 30% of industrial energy consumption worldwide is for heating processes above 700 K. A significant share of fossil fuel consumption is devoted to that

79 aim (also about 30%). However, CSP plants can produce heat in a renewable  
80 way at about those temperatures. Particularly, PDC systems, due to their  
81 high concentration ratio, can well produce heat above 1000 K.

82 In a recent bibliometric analysis within the European project SOLARGRID [13],  
83 Ferruzzi *et al.* [14] consider that solar dishes are still expensive within CSP  
84 technologies (particularly for dish Stirling configurations they mention an  
85 LCoE of 0.26 USD/kWh against an average value of 0.11 USD/kWh for other  
86 CSP technologies) but in their favor have a small footprint, apart from other  
87 advantages as high energy efficiency associated to their high concentration  
88 factor and also their modularity, as mentioned before. These facts make a  
89 continued effort in research and development indispensable to improve tech-  
90 nology competitiveness. Another recent and noteworthy bibliometric study  
91 on solar dishes is due to Ubando *et al.* [15]. It is focused on compiling compu-  
92 tational fluid dynamics (CFD) analysis for solar dish receivers but contains  
93 thorough data on experimental setups, heat transfer fluids, and receiver effi-  
94 ciencies.

95 Probably, the most established markets for PDCs include distributed gen-  
96 eration and remote markets [16]. Applied to electrical power production,  
97 distributed generation refers to that located near the load. From the view-  
98 point of the supply side, its cost competes with that of the base load power.  
99 But close generation can have additional benefits, such improved power qual-  
100 ity and better transmission efficiencies, because of the reduced distances to  
101 save and to avoid building new infrastructures (base-load plants and trans-  
102 mission hardware). However, deploying distributed installations requires an  
103 independent producer to purchase or lease equipment and provide for the  
104 operation and maintenance issues and costs. An essential stimulus for mar-  
105 ket penetration could be open access to the grid and rules allowing to sell  
106 back excess power. Remote markets refer to power installed far from the  
107 grid. These markets include developing countries where national electrical  
108 grids are not fully developed [17] or remote locations with difficult access in  
109 developed countries. Other appealing applications include water pumping  
110 and desalination in arid or desert zones [18, 19], drying [20], integration with  
111 heating and cooling applications in residential buildings [10], thermal energy  
112 storage and hybridization with other renewable energy sources [21, 22]. Re-  
113 quirements for systems devoted to these tasks should include reliability and  
114 ease of maintenance and repair.

115 The energy paradigm is changing towards using renewable energy sources  
116 in the form of electric energy (photovoltaic, wind, hydroelectric). Still, using

117 fuels is almost indispensable for applications with a vast volumetric energy  
118 density. So, the transport sector will continue to rely on combustion engines  
119 using liquid fuels for a long time [23]. The possibility of producing renewable  
120 fuels based on renewable energy sources that could directly replace their fos-  
121 sil counterparts without changing existing infrastructures is appealing. Any  
122 of the processes designed to make those solar fuels is based on two steps:  
123 first, to harvest renewable energy and convert it into usable and second, to  
124 use this energy to produce the fuels from two basic feedstocks, water and  
125 carbon dioxide (see Fig. 7). Possible types of renewable fuels are diverse as  
126 hydrogen [24], syngas (a mixture of CO and H<sub>2</sub>), diesel, and others (methane,  
127 ammonia, etc.). For all of them, there are well-established industrial chem-  
128 ical engineering processes [25], but the significant disadvantage nowadays is  
129 production prices. Within this environment, CSP installations, particularly  
130 solar dishes, can contribute to developing new technological routes for pro-  
131 ducing solar fuels [10, 26].

132 In a broader context, PDCs allow a unique opportunity to use the high  
133 energy and exergy efficiencies of concentrating solar technologies when in-  
134 tegrated or hybridized with advanced systems. This vision article aims to  
135 present an actualized survey on this technology in searching for clean and  
136 renewable electric energy production sources, storage and hybridization, and  
137 heat generation at very different temperature scales with challenging novel  
138 applications. The comprehensive compilation of data, technological options,  
139 and open investigations are interesting for expert and non-expert researchers,  
140 professionals, or other readers. It offers current possibilities and potential  
141 applications of parabolic dish collectors not considered in the available liter-  
142 ature.

143 After a brief comparison with other technologies in Sec. 2, the latest  
144 advances of the main subsystems of a PDC-based plant are presented in Sec.  
145 3, including Stirling, Rankine, and micro-gas turbines. Section 4 surveys  
146 storage and hybridization options, two key advantageous ingredients in CSP  
147 plants to face the main drawbacks of solar irradiance intermittency. Section  
148 5 highlights the applications at different temperature levels, including elec-  
149 tricity generation, domestic and industrial heat requirements, or alternative  
150 routes for producing synthetic fuels due to the high temperatures available  
151 at high concentrator factors. Finally, Sec. 6 summarizes conclusions and  
152 provides a vision of the prospects for this technology.

## 153 2. Costs and comparison with other technologies

154 Several recent studies [27, 28, 29] claim that short and medium-term CSP  
155 deployment dramatically depends on the policies of the governments of differ-  
156 ent countries. The various technologies involved have not reached until now  
157 the minimum technology readiness level (TRL) to freely compete against  
158 others as wind or PV. However, CSP's strong points make it a promising op-  
159 tion for the dispatchable production of renewable energy during the following  
160 years.

161 Specifically, with respect to parabolic dishes, two cost analyses were per-  
162 formed in detail within the OMSoP project (Optimised Microturbine Solar  
163 Power System) [6, 30]. The first one developed a methodology for identifying  
164 potential markets for solar dish Brayton small-scale plants integrating tech-  
165 nical, social, and economic parameters into a figure of merit so-called *index of*  
166 *market potential*. The second one [30] was devoted to analyzing the costs of  
167 developing solar dish installations with micro gas turbines. It was concluded  
168 that specific costs can reach 3300 €/kW<sub>e</sub> on the basis of the construction  
169 of 1000 units for a year but with a wide margin for improvement. It was  
170 also concluded that such technology is more cost-effective than incorporat-  
171 ing Stirling engines instead of micro gas turbines, although more expensive  
172 than a comparable PV installation.

173 In 2020, Zayed *et al.* [31] published a techno-economic analysis of solar  
174 dish Stirling systems located in China with a rated power of 25 kW. A yearly  
175 net overall efficiency of 19.5% was estimated with a simplified model and a  
176 levelized energy cost of 0.26 \$/kWh. Nevertheless, the solar conditions in the  
177 selected location (Tianjin, China) are not especially favorable (around 1200  
178 kWh/m<sup>2</sup>/year).

179 Recent studies from our research group [32, 33] have compared LCoEs  
180 from traditional (non-renewable), other renewable technologies and CSP  
181 plants, including central tower and parabolic dish farms of similar dimen-  
182 sions. In the case of solar dishes for distributed generation with Brayton  
183 cycles (power output between 7 and 30 kW<sub>e</sub>) [33] designed for hybrid oper-  
184 ation with a natural gas combustion chamber for continuous power output,  
185 LCoEs between approximately 0.12 and 0.13 €/kWh<sub>e</sub> were found. The plant  
186 location was Seville in the South of Spain, with good solar resources (around  
187 2000 kWh/m<sup>2</sup>/year). An analysis of the sensitivity of LCoE to fuel cost was  
188 performed, and the role played by recuperation in the Brayton cycle was  
189 surveyed. In [32], an array of solar dishes at power levels between 4.6 and 20

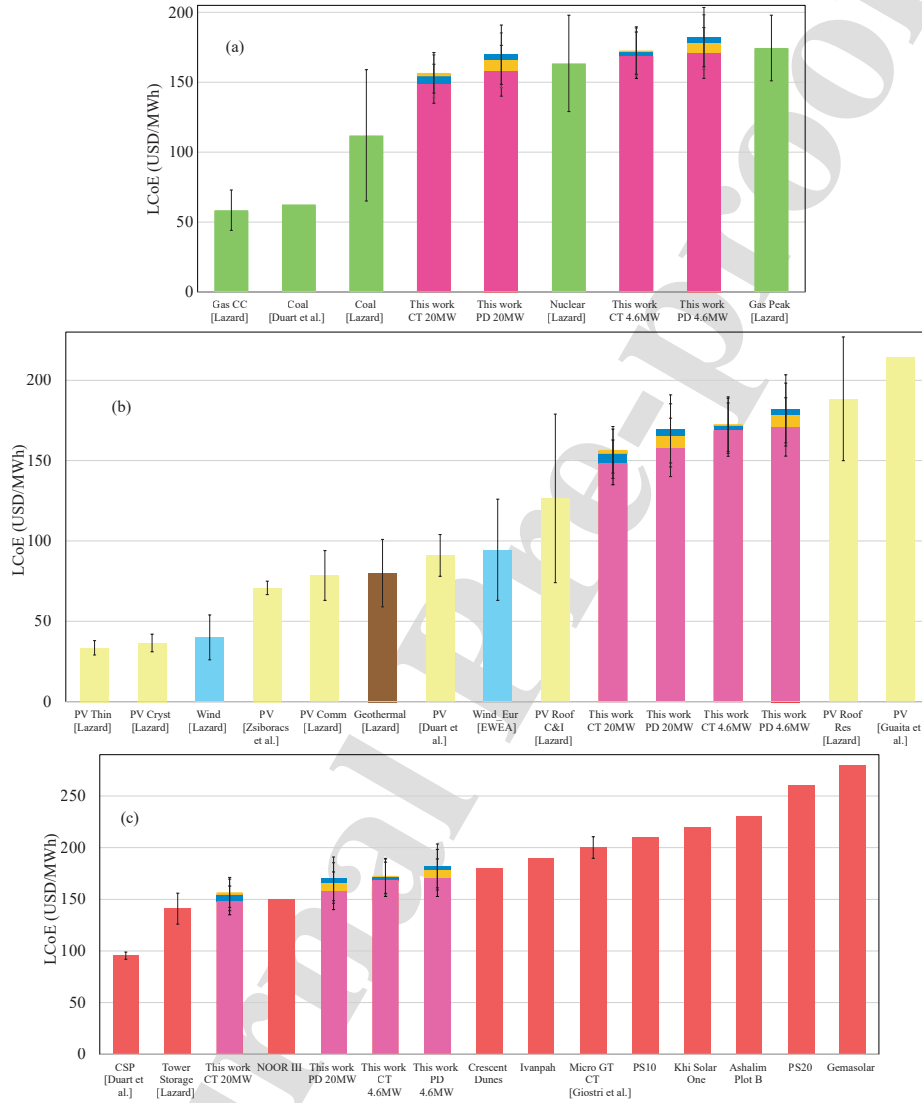


Figure 1: (a) Comparison of LCoE levels from traditional non-renewable plants and medium size parabolic dish (PD) farms and central tower (CT) CSP installations. (b) Analogous comparison of CSP plants against other renewable technologies (geothermal, wind, different PV systems). (c) Comparison of CSP plants from different developed projects, including central towers and parabolic dishes. See details in [32].

190 MW was compared with a central tower plant, working with hybrid Brayton  
 191 cycles and constant power output design. Moreover, LCoE estimations  
 192 were plotted against other traditional and renewable plants for electricity  
 193 production. Figure 1 shows that CSP plants are not so far from other older  
 194 technologies and that arrays of PDCs could compete against medium-sized  
 195 central tower installations. Other economic indicators such as net present  
 196 value, benefit-to-cost ratio, internal rate of return, required land area, and  
 197 discounted payback period were estimated for three locations: Ouarzazate  
 198 (Sahara desert, 2500 kWh/m<sup>2</sup>), Seville and Salamanca (450 km North of  
 199 Seville and about 1800 kWh/m<sup>2</sup>).

### 200 3. Main elements of a PDC-based plant: latest advances

201 This section briefly introduces the latest advances in the subsystems con-  
 202 forming to the PDC, including the solar collector and receiver. If electricity  
 203 is the targeted energy output, a power block is added to the system.

204 The solar collector generally comprises a parabolic reflective surface (usu-  
 205 ally made of stamped mirror facets), a supporting structure for that reflect-  
 206 tive surface, capable of standing the weight and variable wind loads, and the  
 207 tracking system [34]. The most spread tracking system consists of a two-axis  
 208 device that follows the elevation and azimuth Sun coordinates [8].

209 The most relevant enhancements that solar collectors have experienced  
 210 are focused on the mirrored facets geometry and materials. The utmost  
 211 collector geometry concept (for example, the SunCatcher system [35]) is made  
 212 of stamped panels placed in a “petal” (trapezoidal shape facets) arrangement.  
 213 Different combinations of glass, silvered surfaces, and aluminum can be found  
 214 among the reflective materials. The usual configuration covers the front or  
 215 the back surface of glass or plastic with aluminum or silver [36]. Besides,  
 216 reflectivity of 97 % and rim angles near 45° are the most suitable to optimize  
 217 the system [37].

218 Some tools exist to effectively model the parabolic surface and obtain a  
 219 good approach to the actual value of optical efficiency. Ray-tracing software  
 220 has been widely used in the last decade for the optical design of CSP sys-  
 221 tems [38]. This type of software can evaluate the optical performance based  
 222 on the selected material, Sun shape, shading effects, surface errors, receiver  
 223 shape and size, etc. Osorio *et al.* [38] performed a review analysis on the  
 224 most relevant ray-tracing software commonly used. Most of the programs  
 225 reviewed by [38] (Tonatiuh, SolTrace, OTSun, etc.) use the Monte-Carlo

226 method, so they are classified as Monte-Carlo Ray Tracer (MCRT) software.  
227 Other well-known programs are COMSOL [39] and TracePro [40].

228 The solar receiver is one of the most crucial elements within CSP systems  
229 because it defines the maximum achievable temperature [41], thus deter-  
230 mining system efficiency. The solar receiver's function is to turn the solar  
231 irradiance from the collector into usable heat. However, this is not a simple  
232 task. Several heat losses occur during the heat transfer, affecting the receiver  
233 efficiency. Depending on the targeted application, the solar receiver can be  
234 tubular, for generally hosting a liquid HTF [42, 43, 44, 45, 46], or volumet-  
235 ric [47, 48], with gases as HTF and specially devoted to high-temperature  
236 operation

237 The emerging applications for CSP systems, such as the production of  
238 "solar fuels", require high temperatures at the outlet of the receiver [49].  
239 Therefore, the challenging issues for boosting the solar receiver performance  
240 are focused, among others, on geometry, for minimizing heat losses, and  
241 materials, which eventually have to withstand increasingly larger temper-  
242 atures [34, 35] (and so, steep temperature gradients). Solar receivers can  
243 be classified according to different aspects (typology, pressure, temperature  
244 operation levels, heat transfer fluid, etc.).

245 As regards the typology, a solar receiver can be sorted into "external" or  
246 "cavity" configurations, the latter being the most widespread receiver ana-  
247 lyzed in recent studies [12, 24, 41, 49, 50, 51], since they are the most suitable  
248 to withstand temperatures beyond 750°C. In this receiver typology, the solar  
249 irradiance enters the cavity through an aperture area, minimizing convective  
250 and radiative losses. Among the main cavity receiver configurations, tubu-  
251 lar [51, 52], heat pipes [53, 54] and impinging receivers [55, 56] can be found.  
252 Nevertheless, two kinds of cavity receivers are gaining attention: volumetric  
253 and 'absorbing gas' ones.

254 Volumetric receivers are characterized by a volumetric medium (usually  
255 a metallic reticle or ceramic porous foam) that receives the radiative en-  
256 ergy from the Sun. A recent review on pressurized volumetric solar receivers  
257 (paying special attention to parabolic dishes) is due to Belmonte and Tayac-  
258 tac [57]. The HTF flows through the pores and absorbs the thermal energy,  
259 reaching temperatures between 800°C and 1500°C [35], depending on the  
260 material of the porous foam. The HTF, which is generally air, can be used  
261 either to provide thermal energy or be directly used as the working fluid in a  
262 power block such as a gas turbine. Volumetric receivers are pressurized and  
263 closed through a window [35, 58, 59, 60].

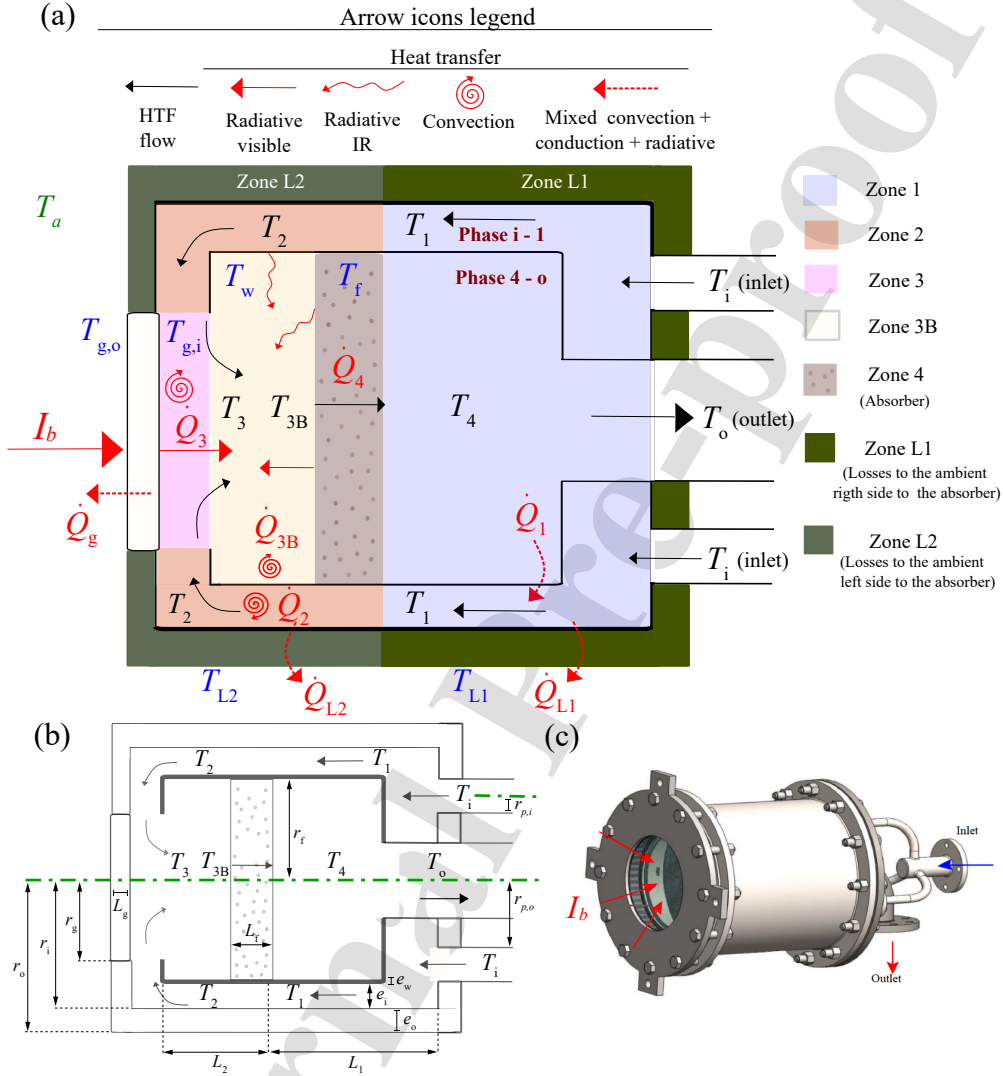


Figure 2: Heat flows and temperatures in a cavity receiver with a metallic absorber foam [47].

264 The receiver thermal efficiency usually ranges between 74% and 87% [60,  
 265 61]. García-Ferrero *et al.* [47] have presented and validated a detailed simulation  
 266 scheme to account for all the realistic losses in the receiver with a  
 267 relatively low computational effort (Fig. 2).

268 Huge efforts have been made for the optimization of the porous medium,

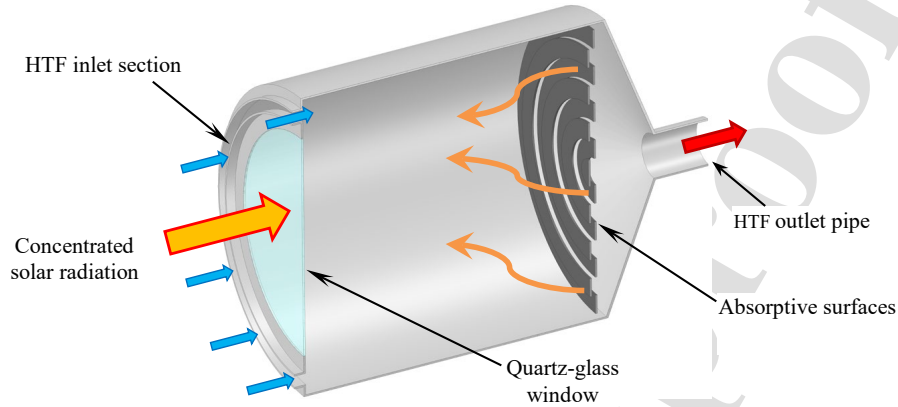


Figure 3: Scheme of the Synhelion absorbing gas receiver working principle [62].

269 aiming to increase the receiver efficiency [63, 64, 65]: simulation techniques  
 270 using Computational Fluids Dynamic (CFD) to demonstrate that thermal  
 271 efficiency strongly depends on the porosity and pore diameter [63], intro-  
 272 ducing the concept of a “gradual decreasing porosity absorber”, that allows  
 273 solar radiation to travel deeper inside the absorber [64] and so, increasing the  
 274 efficiency up to 89% or considering a volumetric effect [65] within the heat  
 275 transfer analysis.

276 Absorbing gas receivers represent a new concept of solar receivers based  
 277 on the properties of some molecular gases to absorb a considerable share of in-  
 278 frared thermal radiation [12, 62]. This principle is similar to the “greenhouse  
 279 effect”. A black surface inside the cavity is stroked by sunbeam radiation that  
 280 is re-emitted and absorbed by the gas. Thus, the gas is heated because of the  
 281 absorption, acting as the HTF (see Fig. 3). Ambrosetti *et al.* [12] proposed  
 282 that concept in their work, modeling the receiver using the spectral line-  
 283 by-line Montecarlo ray tracing method. In a recent work [62], through the  
 284 Synhelion absorbing gas concept, the authors validate the model using CFD  
 285 techniques and under different configurations: pressurized and un-pressurized  
 286 receiver and one or two HTF inlets.

287 PDCs traditionally have been integrated with Stirling engines for gener-  
 288 ating mechanical energy. Among them, there exist kinetic Stirling engines,  
 289 sorted into  $\alpha$ ,  $\beta$  and  $\gamma$  types, attending to the expansion chambers arrange-  
 290 ment and the working gas flow configuration [67, 68, 69, 70, 71]. However,  
 291 there exist other variants: thermoacoustic Stirling engines, where the res-

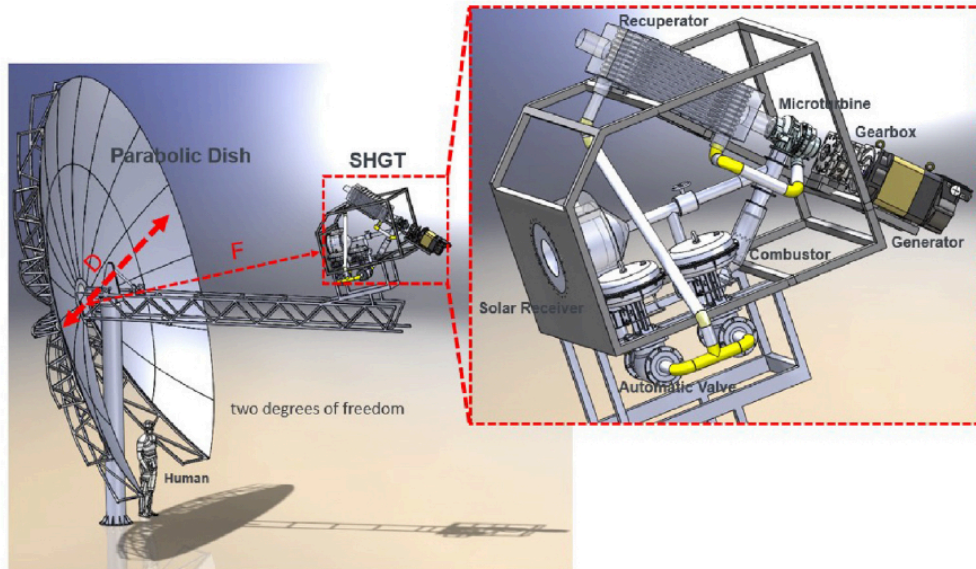


Figure 4: Schematic representation of the possible integration of a recuperative micro-gas turbine (MGT) in a PDC system [66].

292 onance of the acoustic tubes drives the working fluid; free-piston Stirling  
 293 engines, such as the one implemented in Infinia PDC [72]. And finally, liquid  
 294 pistons Stirling engines, where a liquid column replaces the pistons to move  
 295 the working fluid [73]. In the last decade, solar-powered micro-gas turbines  
 296 (MGT) have been considered as a potentially low-maintenance alternative to  
 297 Stirling engines due to gas turbine technology's high production in stationary  
 298 and automotive markets [16, 74, 75]. They can operate in harsh environ-  
 299 ments like deserts or sea sides without needing deep maintenance [76]. The  
 300 main bottleneck for this technology is adapting suitable small turbines for  
 301 solar applications [74]. Because of their compact design, it is not straightfor-  
 302 ward to deal with modifications for integrating the solar receiver [77]. Fig-  
 303 ure 4 displays a possible configuration [66]. MGTs can be applied to parabolic  
 304 solar dishes, providing power outputs up to 50 kW<sub>e</sub> [75]. Recently, Organic  
 305 Rankine Cycles (ORC) have also been considered for producing power at low  
 306 scale (up to 400 W<sub>e</sub> per unit) [78] or as prototype plants [79] to perform  
 307 sensitivity analysis on heat losses and pressure drops, which crucially affect  
 308 the efficiency.

309 Among the working fluids, the air is considered to have many advantages,

310 such as on-site availability, low supply and maintenance costs, no toxicity,  
 311 and absence of environmental problems [80]. Stirling dishes usually employ  
 312 helium as a working fluid, such as Infinia [72] or EuroDISH [81] units, due to  
 313 the suitable power outputs and efficiencies it reports [82]. From an overall  
 314 perspective, solarized open-cycle MGT running with air is one of the best  
 315 configurations for PDCs [83], presenting power block efficiencies between  
 316 27 % and 37 % (at on-design conditions) [83, 84, 85, 86, 87].

#### 317 4. Storage and hybridization trends

318 One of the main drawbacks of thermosolar energy systems is the inter-  
 319 mittency of solar irradiance, which can only be overcome using storage and  
 320 hybridization options. When combined with CSP plants, thermal energy  
 321 storage (TES) leads to more reliable operation and economic feasibility, pro-  
 322 viding dispatchable energy [88]. The hybridization is also of great importance  
 323 to make the system able to be adapted to the energy demand, being the most  
 324 common solution for PDC with a MGT power block [84, 89, 90].

##### 325 4.1. Storage techniques

326 Regarding PDC systems, no standard storage systems are associated with  
 327 the existing/commissioned prototypes [91]. As mentioned, PDC units pro-  
 328 vide small-scale power output (3-50 kW<sub>e</sub>) and compete against PV [92]. PV-  
 329 battery systems offer a reliable energy supply, but recent studies claim that  
 330 the high cost of battery storage is a significant drawback in such a system [93].  
 331 Thus, some theoretical studies are considering different TES coupled to PDC  
 332 for remote and off-grid applications [93, 94].

333 Kee *et al.* [93] proposed the integration of a PDC with a two-tank molten  
 334 salt and a super-critical CO<sub>2</sub> power block (Fig.5(a)). The basic case they  
 335 consider is a power output of 31.5 kW<sub>e</sub>. An overall efficiency of 29.1 % is pre-  
 336 dicted. The LCoE for that power output ranges from 122.7 to 217.8 USD/MWh<sub>e</sub>.  
 337 The authors also simulate a scaled system of 400 kW<sub>e</sub>, finding out that its  
 338 LCoE can be reduced to 121.9 - 172.2 USD/MWh<sub>e</sub>, which can be competitive  
 339 against PV-battery system (LCoE = 180.9 USD/MWh<sub>e</sub>) for locations with  
 340 high annual direct normal irradiance (DNI) resource.

341 Chen *et al.* [96] tested a sensible heat storage of SiC monoliths enclosed in  
 342 a stainless-steel insulated vessel between the solar receiver and the combus-  
 343 tion chamber in a Brayton hybrid configuration. They concluded that storage  
 344 could maintain combustion chamber inlet temperatures above 770°C for more

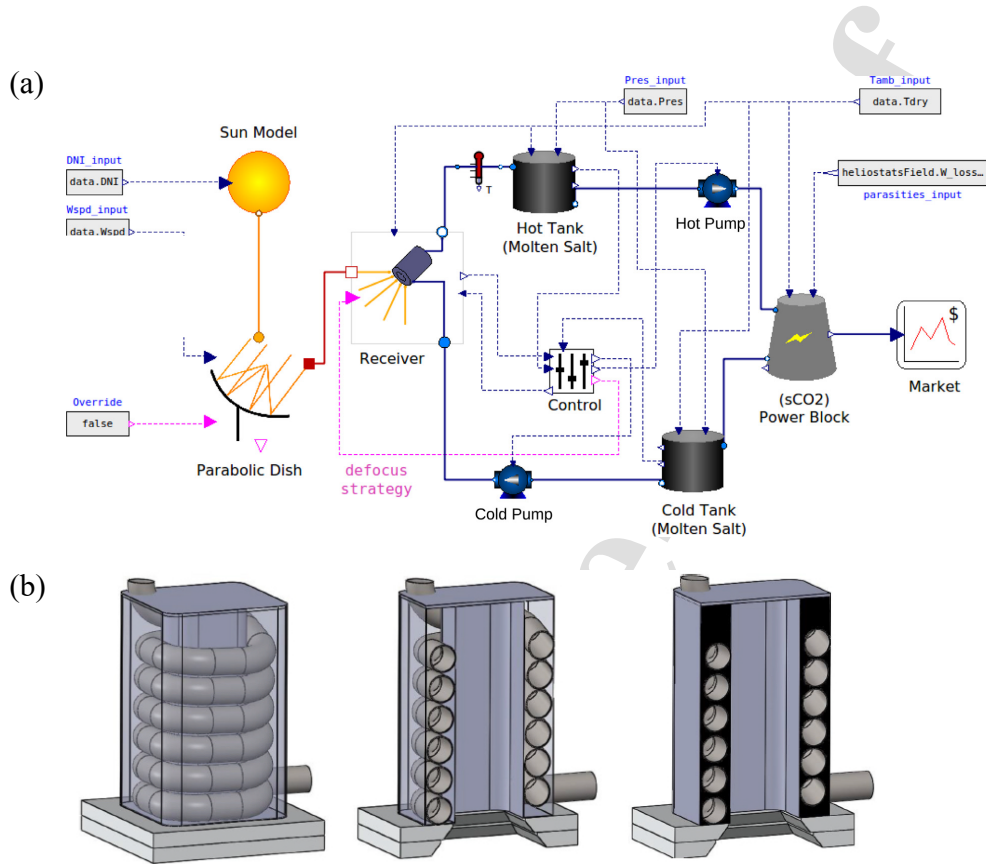


Figure 5: Different energy storage approaches for PDC: (a) PDC + two-tank molten salt + sCO<sub>2</sub> power block [93]; (b) Open-cavity tubular receiver with phase-change material (PCM) storage. From left to right: 3D design, section without PCM material, with PCM material [95].

345 than two hours without solar radiation. Bashir *et al.* [94] designed a tubular  
 346 solar receiver integrated into a MGT - PDC with short-term thermal storage.  
 347 Their work aims to reduce the impact of instant DNI fluctuations, which can  
 348 strongly affect the MGT by suddenly decreasing the working fluid temper-  
 349 ature. Thus, the authors propose using a phase change material (PCM) as  
 350 short-term thermal energy storage (15 - 30 min). The receiver consists of a  
 351 cylinder filled with the PCM and some tubes that contain the HTF flowing  
 352 through them. After the validation and optimization, they obtained a ther-  
 353 mal efficiency of 68 % at on-design conditions. Leroux *et al.* [95] investigated  
 354 an off-the-shelf turbocharger as MGT for low-cost integration into a PDC. An

355 integrated metallic PCM storage was considered in a tubular solar receiver  
356 to improve power stability and performance (see Fig. 5(b)). Solar-to-electric  
357 efficiency reached 21%. Analyses like this one are an open field of research  
358 for the future.

359 Issa *et al.* [97] performed recent experiments focused on analyzing heat  
360 storage from a solar receiver in a PDC. They used an isolated cylindrical  
361 tank with thermosyphon water circulation and different kinds of capsules  
362 containing a PCM material (paraffin wax). Capsules were made of stainless  
363 steel and copper and had different shapes (spherical or cylindrical). Energy  
364 and exergy efficiencies of the storage process were estimated, and very shortly,  
365 it was concluded that copper cylindrical capsules provide an optimal balance  
366 between thermal and storage performance. Defining energy efficiency as the  
367 ratio between the energy stored in the tank (the tank itself, steam, and PCM)  
368 and the energy incident on the receiver, a value of 46.7% was found for copper  
369 capsules.

#### 370 4.2. Hybridization

371 Along with thermal energy storage, hybridization is also a promising op-  
372 tion to enhance PDC's efficiency and flexibility, enabling reliable power gen-  
373 eration [16]. Projects like SOLARGRID consider wide objectives related to  
374 the analysis of hybrid configurations, including solar thermal and PV with  
375 storage for co-generation purposes and flexible generation of energy [13, 14].

376 Semprini *et al.* [84] modeled the integration of a combustion chamber  
377 running with a fossil fuel (natural gas or diesel) into a solarized MGT-PDC.  
378 They analyzed three hybridization strategies: Fuel is supplied for keeping the  
379 power output constant or to ensure an overall efficiency consistently above  
380 a minimum value. The most relevant finding was that the hybrid operation  
381 should be employed during the sunlight hours. Using fossil fuels during the  
382 night is not recommended because the operational cost and carbon footprint  
383 are dramatically increased.

384 Recently, Arifin *et al.* [66] have systematically analyzed hybridization  
385 with a combustion chamber in parallel or serial configurations, either with  
386 internal or external combustion for a MGT-PDC system, in order to develop  
387 well-suited control systems managing fluctuating heat flows in the dynamic  
388 plant operation. They conclude that a parallel configuration where the gas  
389 flow after compression is separated into two branches (one directed to the  
390 solar receiver and another to the combustion chamber) performs better. The  
391 level of solar power input determines the split ratio. García-Ferrero *et al.* [33]

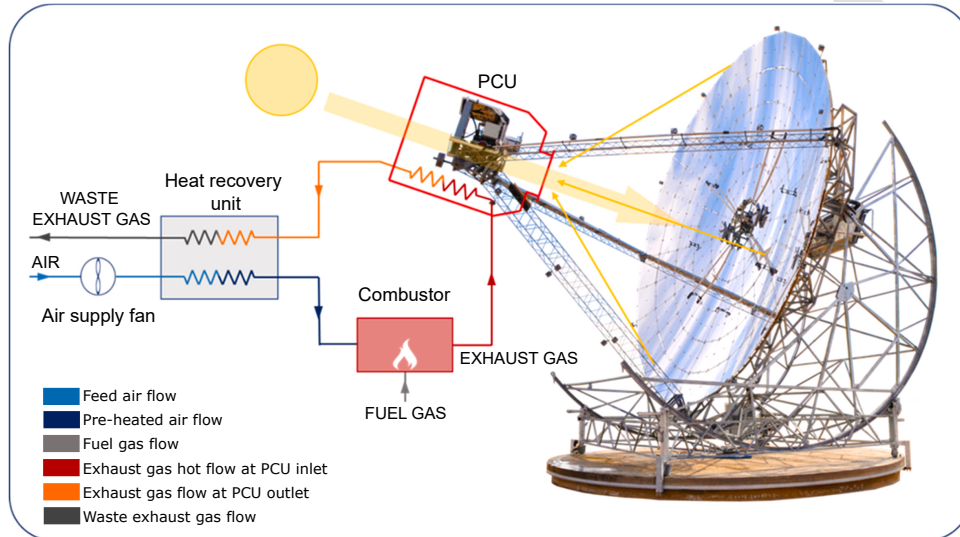


Figure 6: PDC hybrid configuration: dish-Stirling external combustion chamber. Adapted from [16].

392 developed a thermo-economic model for a closed Brayton cycle with external  
 393 combustion in a serial hybrid configuration with an operation aim of keeping  
 394 a power output almost constant. Overall efficiencies around 24% for a 30 kWe  
 395 PDC were found for locations with an annual DNI of about 2000 kWh/m<sup>2</sup>,  
 396 and fuel saving concerning a pure combustion mode reached 30%.

397 Ciulla *et al.* [16], to provide a more realistic approach, modeled the in-  
 398 tegration of a combustion chamber into two actual prototypes (dish-Stirling  
 399 installed at the University of Palermo and the dish-MGT installed at the  
 400 ENEA Casaccia research center). Diverse fuels were analyzed for both sys-  
 401 tems, such as natural gas, syngas or biogas. The main difference relies on  
 402 whether the combustion is internal or external. While Stirling PDC requires  
 403 an external combustion (Fig. 6), MGT could use an internal or external  
 404 combustion chamber. Different locations along the Mediterranean zone were  
 405 studied (Casaccia, Palermo, and Ragusa in Italy, Marrakesh in Morocco,  
 406 and Tabuk in Saudi Arabia), as well as different hybridization scenarios. For  
 407 dish-Stirling, the highest annual solar-to-electric efficiency at solar-only mode  
 408 is obtained at Tabuk (25%). Using syngas or biogas when hybridizing the  
 409 dish-Stirling leads to a CO<sub>2</sub> reduction between 58.3–128 tCO<sub>2</sub>/year. Due to  
 410 the initial design conditions for the dish-MGT, the largest annual solar-to-

411 electric efficiency (in solar-only mode) is obtained in Casaccia (14%). How-  
412 ever, it has a lower DNI resource than Tabuk. Ciulla *et al.* [16] concluded  
413 that, among the different configurations for the combustion chamber in the  
414 solarized-MGT, the internal combustion is about 10 % more efficient for all  
415 the locations and hybridization scenarios considered. The internal combus-  
416 tion of a MGT leads to the utilization of a “clean” fuel gas (natural gas),  
417 avoiding the damage of the components [16]. Biogas fuels could also be em-  
418 ployed within the internal combustion if they were purified [98]. If biogas  
419 is used as fuel for MGT hybridization, the CO<sub>2</sub> avoided will range between  
420 14.1 and 23.3 tCO<sub>2</sub>/year.

421 PDCs are also suitable for hybridization in the broader sense. For ex-  
422 ample, Da Silva *et al.* [99] proposed the integration of wind blades into  
423 a dish-Stirling collector, creating a hybrid solar-wind system. PDCs’ ver-  
424 satility and scalability make them a promising ingredient for multi-source,  
425 multi-generation systems in which different renewable sources (wind, PV,  
426 geothermal. . .) are incorporated together to dispatch in a reliable way heat  
427 (or cold) and power for various purposes, including domestic, industrial, and  
428 others. Nassar *et al.* [100] proposed a hybrid system (hybrid renewable en-  
429 ergy system, HRES) integrating a biomass digester with a Stirling PDC rated  
430 1230 kW. The thermo-economic analysis led to an estimated LCoE of 0.075  
431 \$/kWh and an annual reduction of CO<sub>2</sub> emissions of 7.8 kton.

## 432 5. Innovative applications

433 Solar parabolic dish collectors’ applications focus on spreading from elec-  
434 tricity generation to thermal energy production for different temperature  
435 levels, from low-temperature industrial or domestic heat requirements (or  
436 even heat storage) to novel high-temperature techniques for producing solar  
437 fuels.

438 Low-temperature applications (approximately from 60 to 150°C, see Fig. 2(a))  
439 in [101]) include water treatment, like desalination or distillation, which is a  
440 growing interest topic due to the forecast freshwater stress in developing na-  
441 tions. Many research studies [102, 103, 104, 105, 106] and also some projects  
442 like SOLMIDIFF [107] (see below) are focused on purifying wastewater and  
443 reusing it in industrial processes or taking seawater for turning it into fresh  
444 water. Asadi *et al.* [18] have designed a low-cost unit with a parabolic dish  
445 collector for distillation, investigating different types of basin materials such  
446 as copper, zinc, and iron. The highest thermal efficiency (for copper) reached

447 almost 14%. Esfanjani *et al.* [19] also developed an experimental procedure  
448 for desalination with a PDC using a humidification-dehumidification process.  
449 The authors conclude that the thermal efficiency obtained using a cylindrical-  
450 conical cavity receiver can reach 45.49%. Some innovative approaches are  
451 appearing regarding combined heat and power (CHP) configurations. Al-  
452 Amayreh *et al.* [108] designed a PDC for providing light to indoor PV panels  
453 through optical fibers. The system was also employed for domestic water  
454 heating. Other recent innovative proposals and specific receivers for domes-  
455 tic applications can be found in [109, 110, 111, 112].

456 With respect to the role that solar PDCs can play in the development  
457 of novel energy storage systems, very recently, Palladino *et al.* [113] have  
458 suggested the possible applications of PDC systems as heat generators for  
459 seasonal energy storage applications. Besides, thermochemical energy stor-  
460 age (TCES) options appear, allowing for higher temperature operation and  
461 volumetric energy density. P. Pourmoghadam and M. Mehrpooya [114] in-  
462 vestigated the coupling of a PDC with a TCES unit, using molten salt as  
463 heat transfer fluid in the solar collector and calcium hydroxide,  $\text{Ca}(\text{OH})_2$ , as  
464 TCES material. A Rankine cycle is used for discharging. Energy and exergy  
465 efficiencies were estimated at several locations in Iran. LCoE and payback  
466 period were also calculated. Mohammadi and Merhrpooya [115] have also  
467 suggested the options of PDCs for energy storage through compressed air  
468 energy storage (CAES) plants. Nowadays, CAES tendencies go towards adi-  
469 abatic configurations in which a renewable energy source or a packed-bed  
470 subsystem can heat the air in the discharge phase before entering the expan-  
471 sion turbine. A PDC can provide this heat, contributing to the carbon-free  
472 operation of the plant.

473 As mentioned in Sec. 1, CSP installations, particularly solar dishes, can  
474 contribute to the development of new technological routes for producing solar  
475 fuels [26] taking advantage of the available high temperatures for high concen-  
476 tration factor [26]. Synthetic fuels and biofuels [116] could be an alternative  
477 to achieve a net zero  $\text{CO}_2$  emissions system against well-established indus-  
478 trial chemical engineering processes for hydrogen, syngas, diesel, and others  
479 such as methane and ammonia, although production prices are still high. As  
480 an example, most  $\text{H}_2$  is currently produced via steam methane reforming.  
481 Its production price strongly depends on natural gas prices, but it is about  
482 1.40\$ per kg [23]. Nevertheless, its production through electrolysis with  
483 solar thermal processes is between [3-17]\$ per kg. But, as cited by several  
484 authors [23, 25, 26], sufficient deployment investments for renewable fuel pro-

485 duction may yield learning-by-doing processes that relatively rapidly reduce  
 486 the levelized production costs. In this context, solar dishes could open a new  
 487 technological route for producing solar fuels [26]. A review on biomass gasi-  
 488 fication using concentrated solar collectors is due to Fang *et al.* [117]. They  
 489 argue that efficiencies can reach [25-50]% and are higher than conventional  
 490 gasification processes. Moreover, the potential for reducing feedstock is large.

491  
 492 The scalability and versatility of PDCs (particularly those referring to  
 493 the output temperatures at the solar receiver) make them especially inter-  
 494 esting in exploring new technological routes. Figure 7 illustrates a schematic  
 495 comparison between the current energy supply through fossil resources (left)  
 496 and a possible future strategy that circumvents its use (right) [23]. In the  
 497 latter, the conversion of  $\text{H}_2\text{O}$  and  $\text{CO}_2$  by renewable energy plants allows for  
 498 the production of renewable fuels in a rapid circular scheme that precludes  
 499 the slow fossilization route.

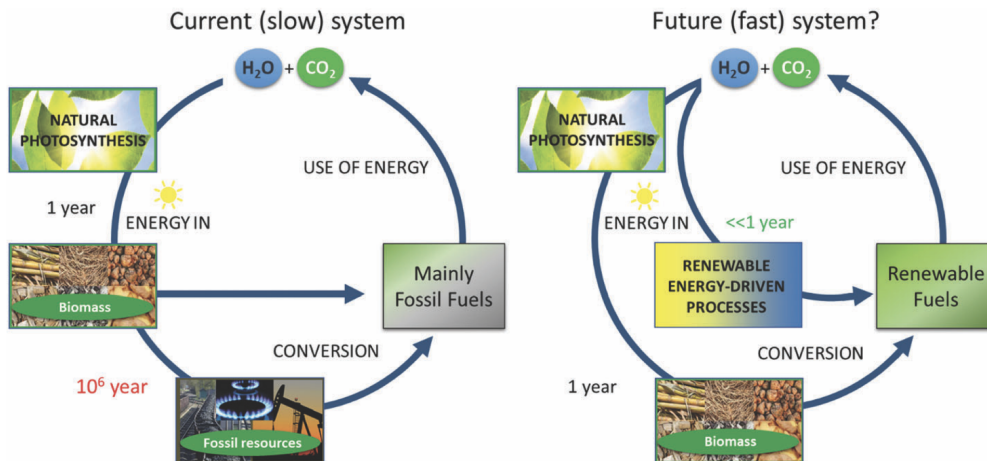


Figure 7: Schematic comparison between current energy supply through fossil resources (left) and a possible future strategy that circumvents its use (right) [23].

500 Figure 8 depicts a recent example for a solar fuel demonstration plant  
 501 installed at ETH in Zurich [26]. Briefly, it has three essential units: the  
 502 direct air capture unit that extracts  $\text{CO}_2$  and  $\text{H}_2$  directly from the ambient,  
 503 the solar redox unit that produces  $\text{CO}$  and  $\text{H}_2$  (syngas) through thermo-  
 504 chemical splitting of  $\text{CO}_2$  and  $\text{H}_2$  via a reduction-oxidation cycle driven by  
 505 concentrated solar radiation, and the gas-to-liquid unit that converts syngas

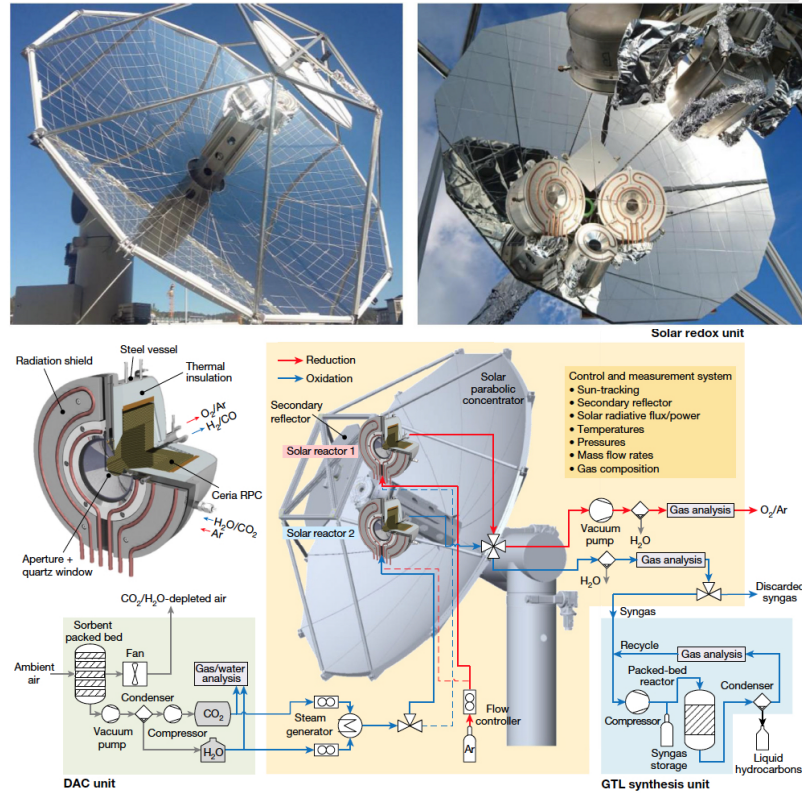


Figure 8: Solar fuel system proposed and proved by Schäppi *et al.* [26]. Up, the image of the final experimental setup built at ETH Zurich, and bottom, scheme of the whole system, including a parabolic dish, a specific solar receiver and the three thermochemical conversion units considered (direct air capture, solar redox unit and gas-to-liquid synthesis unit).

506 to liquid hydrocarbons or methanol. The temperatures required for the re-  
 507 duction step is about  $1500^{\circ}\text{C}$ . The solar reactor is a parabolic dish with a  
 508 cavity receiver, a circular quartz window, and a reticulated porous ceramic.  
 509 For DNIs around  $1000\text{ W/m}^2$ , the receiver can give  $7.7\text{ kW}$  thermal power  
 510 with a concentration of about 2700 suns. The plant is aimed to produce solar  
 511 fuels for air transport, and it is foreseen that it could be scaled up using a  
 512 central tower and a heliostat field with about  $100\text{ MW}_{\text{thermal}}$  to produce mil-  
 513 lions of liters of kerosene per year. System overall efficiency is predicted to  
 514 be around 10%, and the production cost of kerosene per liter is in the range  
 515  $[1.2\text{-}2]\text{\$}$ . To reduce those prices, improving the solar system's performance

would be critical. The authors of the work [26] claim in the conclusions for policy support to get widespread deployment. After demonstrating the actual viability of the technology, scaling, process optimization, mass production of key components, and learning-by-doing are fundamental steps for the next years. Then, synthetic fuels and hydrogen production through PDC are promising applications that are emerging nowadays, mainly in two complementary ways: some authors are focused on thermo-chemical hydrogen production optimizing the solar cavity receiver to enhance the solar-to-fuel conversion efficiency [118]. In contrast, others explore the possibility of electrochemical hydrogen production [119] using novel parabolic dish concentrator geometries and PV modules. Diverse recent studies have focused on this last option [120, 121, 122], considering Stirling dishes due to their high solar-to-hydrogen efficiency (up to 12%). The main drawback of this technology is the high cost it carries, reporting LCoH<sub>2</sub> between 10 -12 \$ /kg, depending on the location. Nevertheless, the hybridization of PV and Stirling dishes leads to promising results, obtaining a compromise between yield production and overall costs.

Several innovative projects devoted to developing different PDC applications for PDCs have been fulfilled recently. A very short summary is presented here. The OMSoP (*Optimised Microturbine Solar Power System*) [123, 124] project was a European project aimed at developing a system able to produce energy for domestic and small-scale applications. SolGATS [125, 126] project intended to analyze a solarized-MGT integrated into a PDC that counted with TES consisting of a ceramic material with a honeycomb structure [127]. SOLMIDIFF (*SOLar Micro gas turbine-driven Desalination for Environmental oFF-grid Applications*) [107] project was devoted to the development of small-scale water desalinization in remote and off-grid locations. Some other projects and initiatives, such as the NextMGT European project or the European MGT Forum, are devoted to enhancing and further commercializing MGT technology into the low carbon economy scenario [128]. SOLARGRID project considers broad objectives related to the analysis of hybrid configurations, including solar thermal and PV with storage for co-generation purposes and flexible generation of energy [13, 14]. Among several solutions, the hybridization of solar dishes in the Mediterranean region was investigated [16].

## 551 6. Conclusions and prospects

552 Nowadays, parabolic dishes are the least developed and commissioned  
553 system among CSP configurations. Therefore, it is clear that this is not a  
554 well-established and marketed technology. More research and development  
555 efforts are required. Some inherent strong points make them promising for  
556 the future. They have a high concentration factor, allowing for high effi-  
557 ciencies and a wide range of temperatures for output heat. Storage and hy-  
558 bridization schemes can be implemented to reduce the fluctuations that most  
559 renewable energy sources have associated with seasonal and meteorological  
560 dynamics. Moreover, their modularity is also a remarkable point. PDCs can  
561 be used for small scale production (distributed generation of electric energy,  
562 domestic applications, etc.) and at medium scale through coupling schemes.

563 Applications are diverse, from the most usual electricity production using  
564 Stirling or Brayton heat devices to heat production at different temper-  
565 atures, all aimed at increasing the use of clean and renewable energies. In  
566 particular, a) low-temperature implementations for water treatment such as  
567 desalination and distillation and the production of domestic heat; and b)  
568 high-temperature applications, for instance, those required for the produc-  
569 tion of synthetic fuels and hydrogen production.

570 PDC-based storage could be an appropriate complement to the photo-  
571 voltaic technology characterized by a direct sunlight conversion with com-  
572 mercial efficiencies from 15% to 22% progressive falling costs but requiring  
573 large areas for significant power generation [129]. Moreover, PDCs can play  
574 an essential role in developing prototypes or R&D&i experiences of technolo-  
575 gies related to energy storage (LAES, CAES, etc.) that can subsequently be  
576 scaled up with other CSP configurations as central tower plants.

577 The solar receiver is the most critical component associated with the solar  
578 PDC. Thus, a fascinating research topic involves its design and configuration,  
579 which strongly depends on the geometry and the type of HTF selected. The  
580 main goal is not only to predict the thermal performance of the receiver ac-  
581 curately but also to find ways to minimize heat losses. Some innovative ideas  
582 to avoid thermal losses imply using coatings, including photonic crystal mir-  
583 rors [130] or transparent aerogels [131]. Nanofluids [132, 133, 134] employed  
584 as HTF in the solar receiver are gaining attention for further enhancing  
585 thermal efficiency, although environmental analysis should be considered to  
586 evaluate the impact of those nanoparticles.

587 Another field that requires deepening in the future is the hybridization

588 of PDCs with other renewable energy sources as wind or PV, for multi-  
589 generation (power, heating, and cooling) purposes in the search for en-  
590 tirely carbon-free, reliable, and predictable schemes for supplying clean en-  
591 ergy [135]. However, caution must be exercised in practical implementation  
592 because integration experiences show that geographic, economic, and climate  
593 changes sometimes require region-specific solutions. Within this context, ad-  
594 vanced control strategies and environmental sustainability assessments (i.e.,  
595 life cycle assessment LCA) are needed to improve the overall performance  
596 and reliability of these systems [10]. However, this research line is out of the  
597 scope of this work, deserving future investigation [136, 137].

598 Moreover, two crucial aspects should be considered when developing this  
599 technology: maintenance, particularly those technical aspects related to soil-  
600 ing, and the economic risk associated with planning the system integration  
601 scenario. Soiling plays a vital role in CSP collectors' performance, especially  
602 those operating in dusty regions. According to [138], energy losses due to  
603 soiling can exceed 17%, which also translates into higher economic costs.  
604 Regarding the PDC integration, they are suitable for distributed energy con-  
605 figurations and off-grid applications. In general, a grid-tied mode is more  
606 economically viable than off-grid applications, except for the case of remote  
607 and scarcely populated locations [139]. From a global perspective, the social,  
608 economic, and environmental factors of a location will influence the feasibility  
609 of the system.

610 In summary, compared to other CSP technologies, PDC could become an  
611 attractive choice for solar power generation due to the high geometric con-  
612 centration factor giving the highest efficiency under nominal conditions, its  
613 modular design allowing adaptability to energy generation at quite different  
614 temperature scales, and its multigeneration capabilities. Opposite, high ini-  
615 tial costs and integration with conventional TES prevent PDC's widespread  
616 market diffusion. Adopting appropriate policies and technological develop-  
617 ment seems necessary for a broad implementation.

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Revised "Highlights"

- Bridged theory and practice by analyzing promising research trends in PDC.
- PDCs have the highest concentration factor, achieving temperatures of about 1000°C.
- Innovative applications for PDCs include CHP, desalination, TES, or solar fuels.
- Integration with smart grids and distributed energy scenarios.
- Feasible storage and hybridization configurations are condensed.

**J. García Ferrero:** Methodology, Investigation, Writing - Original Draft, Writing - Review & Editing.

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**Declaration of interests**

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

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